



# UNIVERSITY OF JOHANNESBURG

## SECOND SEMESTER EXAMINATION 2019

### (SUPPLEMENTARY EXAM)

**COURSE** : MECHANICAL ENGINEERING SCIENCE

**SUBJECT** : MANUFACTURING METHODS 3B

**COURSE CODE:** VVE3B21/VEEMCB3

**TYD/TIME** : 3 hours

**PUNTE/MARKS:** 100

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This paper consists of 4 pages.

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- Requirements : Calculator
  - This examination is closed book.
  - Answer all questions.
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**QUESTION 1****[25]**

- 1.1. Explain the difference between “*roughing*” and “*finishing operations*” in machining (4)
- 1.2. Identify some of the reasons why machining is commercially and technologically important. (4)
- 1.3 Identify the four forces that act upon chips in the orthogonal metal cutting model but cannot be measured directly in an operation. (4)
- 1.4 Highlight the reasons why most welding operations are inherently dangerous (5)
- 1.5 A cutting tool, cutting at 22m/min, gave a life of 1 hour between re-grinds when operating on roughing cuts with mild steel. What will be its probable life when engaged on light finishing cuts?  
Take:  $n = \frac{1}{8}$  for roughening and  $\frac{1}{10}$  for finishing cuts in the Taylor’s equation  $VT^n = C$ . (7)

**QUESTION 2****[20]**

- 2.1 In recent years, conventional machining processes have had to make room for “non-traditional machining processes”. There is a clear distinction between conventional and traditional machining processes. Elaborate on this distinction from a tooling as well as material removal point of view (2)
- 2.2 Highlight FIVE (5) tool-life criteria in production (5)
- 2.3 What is the difference between hot forming and cold forming? (4)

- 2.4 (i) Define Cutting fluid (2)
- (ii) Give the broad classification of fluids and explain them briefly? (4)
- (iii) Enumerate FOUR (4) Functions of cutting Fluid (4)
- 2.5 A plate that is 250 mm wide and 25 mm thick is to be reduced in a single pass in a two-high rolling mill to a thickness of 20 mm. The roll has a radius = 500 mm, and its speed = 30 m/min. The work material has a strength coefficient = 240 MPa and a strain-hardening exponent = 0.2. Determine (a) roll force, (b) roll torque, and (c) power required to accomplish this operation. (4)

### **QUESTION 3** **[20]**

- 3.1. Differentiate between soft “*product variety*” and “hard product variety” (2)
- 3.2. Distinguish between “*direct*” and “*indirect extrusion*”, and also comment about The role of friction on both direct and indirect extrusion (4)
- 3.3. Name some of the steps that can be taken to reduce or eliminate vibration in machining (4)
- 3.4 Briefly explain the following (i) Water jet cutting
- (ii) Abrasive Water jet cutting
- (iii.) Abrasive jet cutting (6)
- 3.4 A single-pass rolling operation reduces a 20-mm-thick plate to 18 mm. The starting plate is 200 mm wide. Roll radius = 250 mm and rotational speed = 12 rev/min. The work metal has a strength coefficient = 600 MPa and a strain hardening exponent = 0.22. Determine (a) roll force, (b) roll torque, and (c) power required for this operation. (6)

**QUESTION 4****[25]**

- 4.1 What are the differences between bulk deformation processes and sheet metal forming? Give TWO (2) examples each. (4)
- 4.2 During inspection and quality testing of welded joints/parts. The following methods were adopted: destructive testing, non-destructive evaluation and visual inspection. Highlight FOUR (4) non-destructive evaluation (NDE) in welding technology. (4)
- 4.3 Define Weldability and state THREE (3) Characteristics of a good weldability (5)
- 4.4 Automation can be defined as the technology by which a process or procedure is performed without human assistance. Humans may be present, but the process itself operates under its own self-direction. Name THREE (3) Components of an Automated system. (3)
- 4.5 Enumerate FOUR (4) Hardware Components of an Automated System (4)
- 4.6 A billet that is 75 mm long with diameter = 35 mm is direct extruded to a diameter of 20 mm. The extrusion die has a die angle =  $75^\circ$ . For the work metal,  $K = 600$  MPa and  $n = 0.25$ . In the Johnson extrusion strain equation,  $a = 0.8$  and  $b = 1.4$ . Determine (a) extrusion ratio, (b) true strain (homogeneous deformation), (c) extrusion strain, and (d) ram pressure and force at  $L = 70$  (5)

## **FORMULA SHEETS**

### **Production Cycle Time Analysis**

$$T_c = T_o + T_h + T_t$$

$$T_b = T_{su} + QT_c$$

$$T_p = \frac{T_{su}}{Q} + T_c = \frac{T_{su} + QT_c}{Q} = \frac{T_b}{Q}$$

$$R_p = \frac{60}{T_p}$$

$$R_c = \frac{60}{T_c}$$

### **Manufacturing Cost Models**

$$C_{pc} = C_m + (C_L + C_{eq})T_p + C_t$$

$$C_L = \frac{R_H}{60} (1 + R_{LOH})$$

$$C_{eq} = \frac{IC}{60NH} (1 + R_{OH})$$

$$Q_o = \frac{Q}{1 - q}$$

### **Material Behaviour in Metal Forming**

$$\sigma = K\epsilon^n$$

$$Y_f = K\epsilon^n$$

$$\bar{Y}_f = \frac{K\epsilon^n}{1 + n}$$

### **Strain Rate Sensitivity**

$$\dot{\epsilon} = \frac{v}{h}$$

$$Y_f = C\dot{\epsilon}^m$$

$$Y_f = A\epsilon^n \dot{\epsilon}^m$$

### **Bulk Deformation Processes in Metalworking**

#### **Rolling**

$$d = t_o - t_f$$

$$r = \frac{d}{t_o}$$

$$t_o w_o L_o = t_f w_f L_f$$

$$t_o w_o v_o = t_f w_f v_f$$

$$s = \frac{v_f - v_r}{v_r}$$

$$\epsilon = \ln \frac{t_o}{t_f}$$

$$\bar{Y}_f = \frac{K\epsilon^n}{1 + n}$$

$$d_{\max} = \mu^2 R$$

$$F = w \int_0^L p dL$$

$$F = \bar{Y}_f w L$$

$$L = \sqrt{R(t_o - t_f)}$$

$$T = 0.5 FL$$

$$P = 2\pi NFL$$

### **Rolling**

$$\epsilon = \ln \frac{h_o}{h}$$

$$F = Y_f A$$

$$F = K_f Y_f A$$

$$K_f = 1 + \frac{0.4 \mu D}{h}$$

### **Extrusion**

$$r_x = \frac{A_o}{A_f}$$

$$\epsilon = \ln r_x = \ln \frac{A_o}{A_f}$$

$$p = \bar{Y}_f \ln r_x$$

$$\bar{Y}_f = \frac{K \epsilon^n}{1 + n}$$

$$\epsilon_x = a + b \ln r_x$$

$$p = \bar{Y}_f \epsilon_x$$

$$\frac{p_f \pi D_o^2}{4} = \mu p_c \pi D_o L$$

$$\mu p_c \pi D_o L = Y_s \pi D_o L$$

$$p_f = \bar{Y}_f \frac{2L}{D_o}$$

$$p = \bar{Y}_f \left( \epsilon_x + \frac{2L}{D_o} \right)$$

$$F = p A_o$$

$$P = Fv$$

$$K_x = 0.98 + 0.02 \left( \frac{C_x}{C_c} \right)^{2.25}$$

$$p = K_x \bar{Y}_f \epsilon_x$$

$$p = K_x \bar{Y}_f \left( \epsilon_x + \frac{2L}{D_o} \right)$$

### **Wire and Bar Drawing**

$$r = \frac{A_o - A_f}{A_o}$$

$$d = D_o - D_f$$

$$\epsilon = \ln \frac{A_o}{A_f} = \ln \frac{1}{1 - r}$$

$$\sigma = \bar{Y}_f \epsilon = \bar{Y}_f \ln \frac{A_o}{A_f}$$

$$\bar{Y}_f = \frac{K \epsilon^n}{1 + n}$$

$$\sigma_d = \bar{Y}_f \left( 1 + \frac{\mu}{\tan \alpha} \right) \phi \ln \frac{A_o}{A_f}$$

$$\phi = 0.88 + 0.12 \frac{D}{L_c}$$

$$D = \frac{D_o + D_f}{2}$$

$$L_c = \frac{D_o - D_f}{2 \sin \alpha}$$

$$F = A_f \sigma_d = A_f \bar{Y}_f \left( 1 + \frac{\mu}{\tan \alpha} \right) \phi \ln \frac{A_o}{A_f}$$

$$\sigma_d = \bar{Y}_f \ln \frac{A_o}{A_f} = Y \ln \frac{A_o}{A_f} = Y \ln \frac{1}{1-r} = Y$$

$$\frac{A_o}{A_f} = e = 2.7183$$

$$r_{\max} = \frac{e-1}{e} = 0.632$$

## **MATERIAL REMOVAL PROCESSES**

### **Theory of metal Machining**

$$R_{MR} = vfd$$

$$r = \frac{t_o}{t_c}$$

$$r = \frac{l_s \sin \phi}{l_s \cos (\phi - \alpha)} = \frac{\sin \phi}{\cos (\phi - \alpha)}$$

$$\tan \phi = \frac{r \cos \alpha}{1 - r \sin \alpha}$$

$$\gamma = \tan (\phi - \alpha) + \cot \phi$$

### **Forces in Metal Cutting**

$$\mu = \frac{F}{N}$$

$$\mu = \tan \beta$$

$$\tau = \frac{F_s}{A_s}$$

$$A_s = \frac{t_o w}{\sin \phi}$$

$$F = F_c \sin \alpha + F_t \cos \alpha$$

$$N = F_c \cos \alpha - F_t \sin \alpha$$

$$F_s = F_c \cos \phi - F_t \sin \phi$$

$$F_n = F_c \sin \phi + F_t \cos \phi$$

$$F_c = \frac{St_o w \cos(\beta - \alpha)}{\sin \phi \cos(\phi + \beta - \alpha)} = \frac{F_s \cos(\beta - \alpha)}{\cos(\phi + \beta - \alpha)}$$

$$F_t = \frac{St_o w \sin(\beta - \alpha)}{\sin \phi \cos(\phi + \beta - \alpha)} = \frac{F_s \sin(\beta - \alpha)}{\cos(\phi + \beta - \alpha)}$$

$$\tau = \frac{F_c \cos \phi - F_t \sin \phi}{(t_o w / \sin \phi)}$$

$$\phi = 45 + \frac{\alpha}{2} - \frac{\beta}{2}$$

### Cutting Tool Technology

$$vT^n = C$$

$$vT^n = C (T_{\text{ref}})^n$$

$$vT^n f^m = K T_{\text{ref}}^n f_{\text{ref}}^m$$

### Economic and Product Design Considerations in Machining

$$R_i = \frac{f^2}{32NR}$$

$$R_a = r_{ai} R_i$$

$$T_c = T_h + T_m + \frac{T_t}{n_p}$$

$$T_m = \frac{\pi DL}{vf}$$

$$n_p = \frac{T}{T_m}$$

$$n_p = \frac{fC^{1/n}}{\pi DLv^{1/n-1}}$$

$$T_c = T_h + \frac{\pi DL}{fv} + \frac{T_t(\pi DLv^{1/n-1})}{fC^{1/n}}$$

$$v_{\text{max}} = \frac{C}{\left[\left(\frac{1}{n} - 1\right) T_t\right]^n}$$

$$T_{\text{max}} = \left(\frac{1}{n} - 1\right) T_t$$

$$C_t = \frac{P_t}{n_e}$$

$$C_t = \frac{P_t}{n_g} + T_g C_g$$

$$C_c = C_o T_h + C_o T_m + \frac{C_o T_t}{n_p} + \frac{C_t}{n_p}$$

$$C_c = C_o T_h + \frac{C_o \pi DL}{fv} + \frac{(C_o T_t + C_t)(\pi DLv^{1/n-1})}{fC^{1/n}}$$

$$v_{\text{min}} = C \left( \frac{n}{1-n} \cdot \frac{C_o}{C_o T_t + C_t} \right)^n$$

$$T_{\text{min}} = \left(\frac{1}{n} - 1\right) \left( \frac{C_o T_t + C_t}{C_o} \right)$$