

PROGRAM	:	BACHELOR OF ENGINEERING TECHNOLOGY (BENGTECH) ENGINEERING : MECHANICAL
<u>SUBJECT</u>	:	STEAM PLANT
<u>CODE</u>	:	SPLM1B2
DATE	:	SUPPLEMENTARY EXAM 09 January 2020
DURATION	:	(SESSION 1) 08:00 - 11:00 (3 hours)
<u>WEIGHT</u>	:	
<u>TOTAL MARKS</u> MAXIMUM MARKS	:	96 = 100% 100
ASSESSOR	:	Mr. E. BAKAYA-KYAHURWA
MODERATOR	:	Mr. S. GQIBANI
NUMBER OF PAGES	:	PAGES: 2 excluding the cover page.
INSTRUCTIONS	:	ONLY ONE POCKET CALCULATOR PER CANDIDATE MAY BE USED.
1. This paper contains	5 qu	lestions
2. PLEASE ANSWER	AL	L the OUESTIONS

- 3. Make sure that you understand what the question requires before attempting it.
- 4. Any additional examination material is to be placed in the answer book and must indicate clearly the question number, and Student number.
- 5. Draw proper sketches where required with all relevant information
- 6. Answers without calculations will not be considered
- 7. Number all answer according to the numbering in question paper.

<u>REQUIREMENTS</u>: Calculator, steam tables, Mollier diagram.

Graduate Attribute:

This assessment is a build up to Graduate Attribute **9**; Independent Learning. Engage in independent and life-long learning through well-developed learning skills.

If required take the specific heat of steam at 1.0 bar (Cps) as 2.1 kJ/kgK

QUESTION 1

- 1.1 The following data was obtained during a trial of a steam boiler at Hendrina power station: Feed water temperature, 75°C. Mass of feed water supplied per hour 4,900 kg. Steam pressure, 11 bar; dryness fraction of steam, 0.9; coal fired per hour, 490 kg; calorific value of 1 kg of dry coal, 35,600 kJ/kg; moisture in coal, 4% on mass basis; temperature of flue gases, 300°C; boiler house temperature, 16°C; barometric (atmospheric) pressure 1.013 bar. Analysis of dry coal on mass basis, C = 89%; H₂ = 3%; ash = 4%; and other matter = 4%; The air fuel ratio required for combustion is 17.7 kg per kg of fuel. Take specific heat of dry flue gases as 1.02 kJ/kg K. Draw up the heat balance sheet for the boiler per kg of coal fired and determine its thermal efficiency. (24)
- 1.2 The steam boiler in this question forms part of a steam plant operating on a Rankine cycle. The steam from the boiler enters the superheater which raises its temperature to 420°C before it expands in turbine and exhausts dry saturated at 10 kPa. For the turbine estimate the turbine power developed and the isentropic efficiency. 10

[34]	
[34]	_

QUESTION 2

A closed vessel of 0.7 m³ capacity contains saturated water vapour and air at a temperature of 42.7°C and pressure of 0.127 bar. Due to further air leakage into the vessel, the pressure rises to 0.28 bar and temperature falls to 37.7°C. Calculate the mass of air which has leaked in. Take R 0.287 kJ/kg K for air.

[10]
[10]

QUESTION 3

- 3.1 Dry saturated steam at a pressure 15 bar expands reversibly in a cylinder behind a piston until the pressure is 1.0 bar. If heat is supplied continuously during the process in order to keep the temperature constant, estimate the change in internal energy per unit mass of steam. [8]
- 3.2 A certain quantity of steam in a closed vessel of fixed volume of 0.3 m³ exerts a pressure of 15 bar at 280°C. If the vessel is cooled so that the pressure falls to 10 bar, evaluate the final quality of steam, and determine the change in internal energy, during the process. [12]

[**20**]

QUESTION 4

A student in the steam plant class carried out an experiment to determine the performance of a cooling tower. The following readings were taken. Estimate the tower characteric and evaluate its effectiveness. Make up water is supplied outside the tower.

inlet dry-bulb temperature (°C)	20.7
air inlet wet bulb temperature (°C)	8
air outlet dry bulb temperature (°C)	21
air outlet wet bulb temperature (°C)	21
water inlet temperature to Tower (°C)	27
water outlet temperature from tower (°C)	15
water flow rate (g/s)	40

[12]

QUESTION 5

A turbine connected to boiler number 4 at Medupi power station, operating, receives steam at 36 bar and 470°C and exhausts at 0.1 bar. At an optimal reheat pressure, the steam is withdrawn and part of it is used for feed water heating in a closed feed heater, while the remainder passes through a reheater. The steam re-enters the turbine at the reheat pressure and 370°C. Evaluate the thermal efficiency of the steam plant taking pump work into consideration. State your assumptions.

[20]
[20]
TOTAL [<u>96</u>]

 $p_{tp} = 611.657 \text{ Pa} = 0.000611657 \text{ MPa}$

p	T _{sat}	Volume,	m ³ /kg	Energ	y, kJ/kg	Ent	halpy, k	J/kg	Entro	py, kJ/s	(kg K)
MPa	°C	v_f	v_g	u_f	u_{g}	h_f	h_q	hfa	Sf.	Sa Sa	Sfo
p_{tp}	0.01	0.00100021	205.991	0	2374.9	0.00	2500.9	2500.9	0	9.1555	9.1555
0.0007	7 1.881	0.00100011	181.217	7.89	2377.4	7.89	2504.3	2496.5	0.02878	9.1058	9.0770
0.0008	3.761	0.00100008	159.640	15.81	2380.1	15.81	2507.8	2492.0	0.05748	9.0567	8.9992
0.0009	5.444	0.00100009	142.757	22.89	2382.4	22.89	2510.9	2488.0	0.08297	9.0135	8.9305
0.0010	6.970	0.00100014	129.178	29.30	2384.5	29.30	2513.7	2484.4	0.10591	8.9749	8.8690
0.0012	9.654	0.00100032	108.670	40.57	2388.2	40.57	2518.6	2478.0	0.14595	8.9082	8.7623
0.0014	11.969	0.00100054	93.899	50.28	2391.3	50.28	2522.8	2472.5	0.18015	8.8521	8.6719
0.0016	14.010	0.00100080	82.743	58.83	2394.1	58.83	2526.5	2467.7	0.21004	8.8035	8.5935
0.0018	15.837	0.00100108	74.011	66.49	2396.7	66.49	2529.9	2463.4	0.23662	8.7608	8.5241
0.0020	17.495	0.00100136	66.987	73.43	2398.9	73.43	2532.9	2459.4	0.26056	8.7226	8.4620
1					1						
0.0024	20.414	0.00100193	56.375	85.65	2402.9	85.65	2538.2	2452.5	0.30239	8.6567	8.3544
0.0028	22.935	0.00100249	48.729	96.19	2406.4	96.19	2542.8	2446.6	0.33816	8.6012	8.2631
0.0032	25.158	0.00100305	42.952	105.49	2409.4	105.49	2546.8	2441.3	0.36945	8.5533	8.1838
0.0036	27.152	0.00100358	38.430	113.83	2412.1	113.83	2550.4	2436.6	0.39729	8.5110	8.1138
0.0040	28.960	0.00100410	34.791	121.39	2414.5	121.39	2553.7	2432.3	0.42239	8.4734	8.0510
0.0045	31.012	0.00100473	31.131	129.96	2417.3	129.96	2557.4	2427.4	0.45069	8.4313	7.9806
0.0050	32.874	0.00100533	28.185	137.74	2419.8	137.75	2560.7	2423.0	0.47620	8.3938	7.9176
0.0055	34.581	0.00100590	25.762	144.87	2422.1	144.88	2563.8	2418.9	0.49945	8.3599	7.8605
0.0060	36.159	0.00100645	23.733	151.47	2424.2	151.48	2566.6	2415.2	0.52082	8.3290	7.8082
0.0065	37.627	0.00100699	22.009	157.60	2426.2	157.61	2569.3	2411.6	0.54060	8.3007	7.7601
	1										
0.0070	39.000	0.00100750	20.524	163.34	2428.0	163.35	2571.7	2408.4	0.55903	8.2745	7.7154
0.0075	40.290	0.00100800	19.233	168.74	2429.8	168.75	2574.0	2405.3	0.57627	8.2501	7.6738
0.0080	41.509	0.00100848	18.099	173.83	2431.4	173.84	2576.2	2402.4	0.59249	8.2273	7.6348
0.0085	42.663	0.00100895	17.095	178.66	2433.0	178.67	2578.3	2399.6	0.60780	8.2060	7.5982
0.0090	43.761	0.00100940	16.199	183.24	2434.4	183.25	2580.2	2397.0	0.62230	8.1858	7.5635
0.0095	44.807	0.00100984	15.396	187.62	2435.8	187.63	2582.1	2394.5	0.63607	8.1668	7.5308
0.010	45.806	0.00101027	14.670	191.80	2437.2	191.81	2583.9	2392.1	0.64920	8.1488	7.4996
0.011	47.683	0.00101110	13.412	199.64	2439.7	199.65	2587.2	2387.5	0.67372	8.1154	7.4417
0.012	49.419	0.00101188	12.358	206.90	2442.0	206.91	2590.3	2383.4	0.69628	8.0849	7.3887
0.013	51.034	0.00101263	11.462	213.66	2444.1	213.67	2593.1	2379.4	0.71717	8.0570	7.3398
0.014	52.547	0.00101335	10.691	219.98	2446.1	219.99	2595.8	2375.8	0.73664	8.0311	7.2945
0.016	55.313	0.00101471	9.4306	231.55	2449.7	231.57	2600.6	2369.1	0.77201	7.9846	7.2126
0.018	57.798	0.00101597	8.4431	241.94	2453.0	241.96	2605.0	2363.0	0.80355	7.9437	7.1402
0.020	60.058	0.00101716	7.6480	251.40	2455.9	251.42	2608.9	2357.5	0.83202	7.9072	7.0752
0.024	64.053	0.00101934	6.4453	268.13	2461.2	268.15	2615.9	2347.7	0.88191	7.8442	6.9623
0.028	67.518	0.00102131	5.5778	282.63	2465.6	282.66	2621.8	2339.2	0.92472	7.7912	6.8664
0.032	70.586	0.00102312	4.9215	295.49	2469.6	295.52	2627.1	2331.6	0.96228	7.7453	6.7830
0.036	73.345	0.00102480	4.4072	307.05	2473.1	307.09	2631.8	2324.7	0.99579	7.7050	6.7092
0.040	75.857	0.00102638	3.9930	317.58	2476.4	317.62	2636.1	2318.4	1.0261	7.6690	6.6429
0.045	78.715	0.00102821	3.5759	329.57	2480.0	329.62	2640.9	2311.2	1.0603	7.6288	6.5686
0.050	81.317	0.00102993	3.2400	340.49	2483.2	340.54	2645.2	2304.7	1.0912	7.5930	6.5018

Continued ...

Saturated Water and Steam (Pressure-based), Contd.

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p	$T_{\rm sat}$	Volume, r	n ³ /kg	Energy	, kJ/kg	Enth	alpy, k.	J/kg	Entro	py, kJ/(kg K)
MPa	°C	v_f	v_g	u_f	u_g	h_{f}	h_g	h_{fg}	s_f	s_g	s_{fg}
0.050	81.317	0.00102993	3.2400	340.49	2483.2	340.54	2645.2	2304.7	1.0912	7.5930	6.5018
0.055	83.709	0.00103154	2.9635	350.53	2486.2	350.59	2649.2	2298.6	1.1194	7.5606	6.4412
0.060	85.926	0.00103307	2.7317	359.85	2489.0	359.91	2652.9	2292.9	1.1454	7.5311	6.3857
0.065	87.993	0.00103452	2.5346	368.53	2491.6	368.60	2656.3	2287.7	1.1696	7.5040	6.3345
0.070	89.932	0.00103590	2.3648	376.68	2493.9	376.75	2659.4	2282.7	1.1921	7.4790	6.2869
0.075	91.758	0.00103723	2.2170	384.36	2496.1	384.44	2662.4	2277.9	1.2132	7.4557	6.2425
0.080	93.486	0.00103850	2.0871	391.63	2498.2	391.71	2665.2	2273.5	1.2330	7.4339	6.2009
0.085	95.125	0.00103972	1.9720	398.53	2500.2	398.62	2667.8	2269.2	1.2518	7.4135	6.1617
0.090	96.687	0.00104091	1.8694	405.11	2502.1	405.20	2670.3	2265.1	1.2696	7.3943	6.1246
0.095	98.178	0.00104205	1.7772	411.38	2503.9	411.48	2672.7	2261.2	1.2866	7.3761	6.0895
0.10	99.606	0.00104315	1.6939	417.40	2505.5	417.50	2674.9	2257.4	1.3028	7.3588	6.0561
0.11	102.292	0.00104527	1.5495	428.73	2508.8	428.84	2679.2	2250.3	1.3330	7.3269	5.9938
0.12	104.784	0.00104727	1.4284	439.23	2511.7	439.36	2683.1	2243.7	1.3609	7.2977	5.9367
0.13	107.109	0.00104917	1.3253	449.05	2514.3	449.19	2686.6	2237.5	1.3868	7.2709	5.8840
0.14	109.292	0.00105099	1.2366	458.27	2516.9	458.42	2690.0	2231.6	1.4110	7.2461	5.8351
0.15	111.349	0.00105273	1.1593	466.97	2519.2	467.13	2693.1	2226.0	1.4337	7.2230	5.7893
0.16	113.297	0.00105440	1.0914	475.21	2521.4	475.38	2696.0	2220.7	1.4551	7.2014	5.7463
0.17	115.148	0.00105600	1.0312	483.04	2523.5	483.22	2698.8	2215.6	1.4753	7.1812	5.7059
0.18	116.911	0.00105756	0.97747	490.51	2525.5	490.70	2701.4	2210.7	1.4945	7.1621	5.6676
0.19	118.596	0.00105906	0.92924	497.65	2527.3	497.85	2703.9	2206.0	1.5127	7.1440	5.6313
0.20	120.210	0.00106052	0.88568	504.49	2529.1	504.70	2706.2	2201.5	1.5302	7.1269	5.5967
0.21	121.759	0.00106193	0.84614	511.07	2530.8	511.29	2708.5	2197.2	1.5469	7.1106	5.5638
0.22	123.250	0.00106330	0.81007	517.40	2532.4	517.63	2710.6	2193.0	1.5628	7.0951	5.5323
0.23	124.686	0.00106464	0.77704	523.50	2534.0	523.74	2712.7	2188.9	1.5782	7.0803	5.5021
0.24	126.072	0.00106594	0.74668	529.38	2535.4	529.64	2714.6	2185.0	1.5930	7.0661	5.4731
0.25	127.411	0.00106722	0.71866	535.07	2536.8	535.34	2716.5	2181.1	1.6072	7.0524	5.4452
0.26	128.708	0.00106846	0.69273	540.59	2538.2	540.87	2718.3	2177.4	1.6210	7.0394	5.4184
0.27	129.965	0.00106968	0.66865	545.95	2539.5	546.24	2720.0	2173.8	1.6343	7.0268	5.3925
0.28	131.185	0.00107086	0.64624	551.14	2540.8	551.44	2721.7	2170.3	1.6471	7.0146	5.3675
0.29	132.370	0.00107203	0.62533	556.19	2542.0	556.50	2723.3	2166.8	1.6596	7.0029	5.3433
0.30	133.522	0.00107317	0.60576	561.11	2543.2	561.43	2724.9	2163.5	1.6717	6.9916	5.3199
0.31	134.644	0.00107429	0.58741	565.89	2544.3	566.22	2726.4	2160.2	1.6835	6.9807	5.2972
0.32	135.737	0.00107539	0.57017	570.56	2545.3	570.90	2727.8	2157.0	1.6949	6.9701	5.2752
0.33	136.802	0.00107647	0.55395	575.10	2546.5	575.46	2729.3	2153.8	1.7060	6.9598	5.2538
0.34	137.842	0.00107753	0.53864	579.54	2547.5	579.91	2730.6	2150.7	1.7168	6.9498	5.2330
0.35	138.857	0.00107857	0.52418	583.88	2548.5	584.26	2732.0	2147.7	1.7274	6.9401	5.2128
0.36	139.849	0.00107960	0.51050	588.13	2549.4	588.52	2733.2	2144.7	1.7377	6.9307	5.1931
0.37	140.819	0.00108061	0.49753	592.28	2550.4	592.68	2734.5	2141.8	1.7477	6.9216	5.1739
0.38	141.769	0.00108161	0.48522	596.34	2551.3	596.75	2735.7	2139.0	1.7575	6.9126	5.1551
0.39	142.698	0.00108259	0.47352	600.32	2552.2	600.74	2736.9	2136.2	1.7671	6.9040	5.1369
0.40	143.608	0.00108355	0.46238	604.22	2553.1	604.65	2738.1	2133.4	1.7765	6.8955	5.1190

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hosen to be zei	1.01325	0.8453	0.7/80	0.4736	0.1055	0.2501	0.1574 0.1992	0.1233	0.1116	0.1009	0.08198	0.06624	0.05940	0.04754 0.04754 0.04318	0.04004	0.03778	0.03360	0.02982	0.02808	0.02337	0.02196	0.01936	0.01704 0.01817	0.01597	0.01401	0.01227	0.01147	0.01001	0.008719 0.009346	0.008129	0.007054	0.006112	[bar]
ro for saturated	1.673	1.982	2.828	4,133 3,408	1122	6.201	9.578	12.04	13.23	16.03	17.69	21.63	23.97	29.57	34.77	36.73	41.03	45.92	51,49 48,62	54.56	61.34	65.09	77.97	82.89	93.83 88.17	106.4 99.90	113.4	129.1 121.0	147.1 137.8	157.3	179.9	206.1	m~/881
l liquid at th	419.1 2	398.0	225.9	313.9 334.9 2	- VCF7	272.0	230.2	209.3	200.9	194.2	175.8	159.1	150.7	134.0	121.5	117.3	104.8	100.6	922 2	88.0	79,7	71.3	6 <u>2</u> 9	58.8	4 8	42.0	37.8	29,4 33,6	21.0 25.2	16.8		9	
e triple point	256.7 20	269.8 20	1295.6	132018 1308.3 20	2000 2	345.7 20	1370.1 1357.9 20	382.1 2	387.0 2	1396.6 296.7	406.2 2	2411.0 2	415.8 2	430.0 2	432.4 2	437.2 2: 434.8 2:	2441.8 2 2439.5 2	444.2 2	2449.0 2 446.6 2	2453.7 2 2451.4 2	456.0 2	2460.8 2:	2465.5 22 2463.1 22	2467.8 2	472.5 2470.5 2	2477.2 2 2474.9 2	2479.6 2	2484.3 2 2481.9 2	2488.9 2 2486.6 2	2491,3 2	2498.3 2	2500.8 2	[KJ/Kg]
	575.8	67.8	51.5	543.2	C.070	517.7	500	591.4	587.9	580.8	573.7	570.1	2,995	555.7	553.9	550.3	546.6	544.8	541.2	537.6 539.4	535.7	532.1	528.4 530.2	526.6	522.9 574 8	519.2 S21.1	517.4	513.7	509.9	508.1		500.8	
	1.307 6.	1.250 6.	1.134 6.	1.075 6.	0.900 6.	0.893 6	0.768 7.	0.704 7.	0.678 7.	0.625 7.	0.572 7.	0.545 7.	0.518 7.	0.436 8.	0,423 8.	0.395 8.	0.367 8	0.353 8.	0.325 8	0.296 8.	0.282 8.	0.253 8	0.224 8	0.210 8	0.180	0.151 8	0.136 8		0.076 8	0.046 9	0.031 9	9	[1]
	048 7.35	260 <i>1.41</i> 166 7.41	410 7.54	536 7.68	C/ DUR	937 7.83	223 7.99	371 8.07	433 8.11	557 8.18	684 8.25 620 8.21	749 8.29	814 8.33	016 8,45 948 8,41	050 8.47	120 8.51	190 8.53 155 8.53	226 8.57	297 8.62	370 8.66 334 8.64	407 8.68	481 8.73	556 8.78 518 8.75	594 8.80	671 8.85	749 8.90	.788 8.92	8068 8.97 8.97	9.03 9.03	.989 9.05 9.05	.071 9.12	.155 9.1:	kg K]
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	. 1																												e,				
		1.00 26.0	0.90	0.80	0.75	0.70	8	0.55	0.50	0.46	0.42 0.44	0.40	0.36	0.32 0.34	0.30	0.26	0.22	0.20	0.16	0.12	0.095	0.090	0.080	0.070	0.065	0.055	0.045	0.040	0.030	0.020	0.010	0.006112	[bar]
		98.2 98.2	83	93.5	91.8	90.0 88.0	86.0	93 7	88 13 13 13	79.3	77.1	75.9	124	70.6	67.5 69.1	65.9	6 2 2	57.8 60.1	SS.	49.4 52.6	44,8 45,8	43.8	517	40.3	37.7	34.6	31.0 32.9	26.7 29.0	24.1	17.5	7.0	0.01	3

Note: values of pr can be found on p. 10.

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T. w. w.<	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	10C2 62F2 5
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Ti Win Min <td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td> <td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td> <td>2470 252</td>	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	2470 252
p T _h u _B u _I u _B u	P T ₁ V _B M ₁ M ₂ I [bar] [°C] [m ³ /kg] [LJ/kg] [LJ/kg] I 0.006112 0.01 206.1 0† 2375 I	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0 7485 751
$ \begin{array}{c c} p & T_{h} & v_{g} \\ \hline \begin{array}{c} \text{[bar]} & \hline (C] & \hline (m^{3})kg \\ \end{array} \end{array} \begin{array}{c} u_{f} & u_{h} \\ \hline \begin{array}{c} kJ/kg \\ \end{array} \end{array} $	$ \begin{array}{c c} p & T_{1} & v_{2} \\ \hline \hline bar \\ \hline bar \\ \hline \end{array} \begin{array}{c} T_{1} & v_{2} \\ \hline \hline c \\ \hline c \\ \end{array} \begin{array}{c} v_{1} & v_{2} \\ \hline \hline c \\ \hline c \\ \end{array} \begin{array}{c} u_{1} & u_{1} \\ \hline c \\ \hline c \\ \hline c \\ \end{array} \begin{array}{c} u_{1} & u_{2} \\ \hline c \\ \hline c \\ \end{array} \begin{array}{c} u_{1} & u_{2} \\ \hline c \\ \hline c \\ \end{array} \end{array} $	$ \begin{array}{c c} p & T_{1} & v_{g} \\ \hline \ \ \ \ \ \ \ \ \ \ \ \ \$	0* 2501 250
			[kJ/kg]

Saturated Water and Steam

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2014	2214 2196 2174 2146 2097	2283 2271 2259 2245 2231	2375 2339 2339 2318 2294	2445 2420 2406 2391	2496 2487 2467 2456	2537 2529 2522 2514 2514	2555 2555 2555	2594 2586 2581 2581	2601 2600 2599 2598 2597	^{ال} و] 1602
2084	1904 1921 1940 2008	1838 1849 1861 1874 1889	1732 1754 1777 1801 1827	1630 1650 1670 1711	1531 1551 1591 1610	1429 1450 1511	1317 1341 1364 1408	1185 1214 1241 1267 1293	1102 11129 11155	1087
0	412 373 270 170	447985556	584 584	967 895 819	1034 1001	11224 11224 11924	1441 1410 1379 1348	1605 1570 1538 1473	1698 1683 1683 1654	h _{fs} [kJ/kg] 1714
2084	2316 2294 2235 2178	22259 22369 22369	2510 2489 2440 2440 2411	2548 2530	2662 2650 2638 2611	27115 2705 2695 2685 2674	2758 2751 2743 2734 2734 2734	2790 2784 2779 2772 2766	2800 2798 2797 2796 2794	2801
4.406	4.131 4.157 4.186 4.224 4.289	4.031 4.067 4.108	3.872 3.905 3.941 3.977 4.014	3.715 3.746 3.777 3.808 3.839	3.561 3.592 3.623 3.654 3.685	3.395 3.430 3.496 3.529	3.207 3.248 3.286 3.324 3.360	2.976 3.027 3.122 3.166	2.823 2.849 2.874 2.874 2.897 2.921	2,797
0.000	0.640 0.579 0.417	0.875 0.792 0.745 0.695	1.236 1.163 1.086 1.004 0.914	1.305 1.305	1.872 1.811 1.689 1.627	2.189 2.123 2.060 1.997 1.934	2.537 2.463 2.393 2.325 2.255	2955 2863 2775 2692 2613	3.226 3.180 3.094 3.052	^{Srg} KJ/kg K.] 3.273
4.406	4.771 4.736 4.694 4.552	4.884 4.859 4.832	5.108 5.068 5.027 4.981 4.928	5.280 5.248 5.181 5.144	5,403 5,343 5,343	5.584 5.523 5.493 5.463	5.714 5.711 5.679 5.647 5.615	5.931 5.890 5.851 5.814 5.779	6.049 6.029 5.991 5.973	6.070

Saturated Water and Steam

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† The entries should be div this has not this has not this has not the point of	4 (143.6)	3 (133.5)	2 (120.2)	(111.4)	1.01325 (100.0)	1 (99.6)	0.75 (91.8)	0.5 (81.3)	0.1 (45.8)	0.05 (32.9)	0.01 (7.0)	0.006112 (0.01)	0	p/[bar] (7,/[°C])	Superheat
in all tables are ided by the app seen done consis 3.	r= 0.4623 H= 2554 H= 2739 S= 6.897	0,6057 0,2544 1,2725 3,6,993	0.8856 u 2530 h 2707 s 7.127	v, 1.159 u, 2519 h, 2693 s, 7.223	v, 1.673 u, 2506 h, 2676 s, 7.355	r 1.694 4 2506 5 7.359	r: 2.217 ¹ / ₂ 2496 ¹ / ₂ 2662 ⁵ / ₂ 7.456	r: 3.239 u: 2483 h: 2645 s: 7.593	e: 14.67 u: 2437 h: 2584 s: 8.149	v _s 28.20 ^u s 2420 ^s 8.394	μ _{129,2} μ ₂₂₃₈₅ μ ₂₅₁₄ s _{8,974}	v _s 206.1 u _s 2375 h _z 2501 s _s 9.155	u = h - RT at $p = 0$		ed Steamt
regarded propriate stently in		* 37 5 7	r 3-E 4	* 7 5 7	0 7 E G	8 3 -E 7	N 37 5 7	. 32.	5 Z Z T	N 3-E C		N 27 E 11	5 3- E C	r <u>[]</u>	
as pure units as the supe	<u>6666</u> 								14.87 2443 2592 8.173	29.78 2445 2594 8.496	149.1 2446 2595 9.241	243.9 2446 9.468 9.468	2446 2595	8	
numben shown f rheat ar						1.696 2506 2676 7.360	2.271 2510 2680 7.500	3,420 2512 2683 7,694	17.20 2516 2688 8.447	34,42 2516 2688 8.768	172.2 2517 2689 9.512	281.7 2517 2689 9.739	2517 2689	100	
s and the or the e nd super	0.4710 2565 2753 6.929	0.6342 2572 2762 7.078	0,9602 2578 2770 7,280	1.286 2580 2773 7.420	1.912 2583 2777 7.608	1.937 2583 2777 7.614	2,588 2585 2779 7.750	3.890 2585 7.940	19.51 2588 2783 8.688	39.04 2589 9.008	195.3 2589 2784 9.751	319.5 2589 2784 9.978	2589 2784	150	
erefore th ntries at / critical t	0.5345 2648 2862 7.172	0,7166 2651 2866 7,312	1.081 2655 2871 7.507	1,445 2656 7,643	2.145 2659 2876 7.828	2.173 2659 2876 7.834	2.901 2659 2877 7.969	4.356 2660 2878 8.158	21.83 2662 2880 8.903	43,66 2662 9,223	218,4 2662 2880 9.966	357.3 2662 2880 10.193	2662 2880	200	
ne symbo p/[bar] = ables on	0.5953 2727 2965 7.379	0.7965 2729 2968 7.517	1,199 2731 2971 7,708	1.601 2733 2973 7.843	2.375 2734 2975 8.027	2,406 27734 2,975 8,033	3.211 2734 2975 8.167	4.821 2735 2976 8.355	24.14 2736 2977 9.100	48.28 2737 2978 9.420	241.4 2737 2978 10.163	395.0 2737 2978 10.390	2737 2978	250	
ls for the 4. Becau pp. 6-9 a	0.6549 2805 3067 7.566	0.8754 2807 3070 7.702	1.316 2809 3072 7.892	1.757 2809 3073 8.027	2.604 2811 3075 8.209	2,639 2811 3075 8,215	3.521 2811 3075 8.349	5.284 2812 3076 8.537	26,45 2812 9,281	52.90 2812 9.601	264.5 2812 3077 10.344	432.8 2812 3077	2812 3077	300	
physical se of lack and in the	0.7725 2965 3274 7.898	1,031 2966 3275 8,032	1.549 2967 3277 8.221	2.067 2967 3277 8.355	3.062 2968 3278 8.537	3.103 2968 3278 8.543	4.138 2969 3279 8.676	6.209 2969 3279 8.864	31.06 2969 3280 9.607	62.13 2969 3280 9.927	310.7 2969 3280 10.670	508.3 2969 3280 10.897	2969 3280	400	
quantities c of space tables or	0.8893 3129 3485 8.191	1.187 3130 3486 8.324	1.781 3131 3487 8.513	2,376 3131 3488 8.646	3.519 3131 3488 8.828	3.565 3131 3488 8.834	4.755 3132 3489 8.967	7.134 3132 3489 9.154	35.68 3132 3489 9.897	71.36 3132 3489 10.217	356.8 3132 3489 10.960	583.8 3132 3489 11.187	3132 3489	SOO	
*See footn	70 (285.8)	60 (275.6)	50 (263.9)	40 (250.3)	30 (233.8)	20 (212,4)	15 (198.3)	10 (179.9)	9 (175.4)	8 (170,4)	7 (165.0)	6 (158.8)	5 (151.8)	<i>p/</i> [bar] (7,/[مر])	
* See footnote on p	70 (285.8) <i>S</i> <i>S</i>	60 (275.6) <i>h</i> ^g <i>h</i> ^g	$\begin{array}{c} 50 \\ (263.9) \\ s_{g} \\ s_{g} \end{array}$	$\begin{array}{c} 40 \\ (250.3) \\ S_{\rm R} \\ S_{\rm R} \end{array}$	$\begin{array}{c} 30\\ u_{x}\\ (233.8) \\ J_{x}\\ S_{x}\\ S_{x}\end{array}$	$\begin{array}{c} 20 \\ 12.4 \\ 3_{\text{B}} \\ 3_{\text{B}} \end{array}$	15 (198.3)	10 4 4 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 2, (175.4) 4, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5,	(170.4) $\begin{pmatrix} v_{s} \\ k_{s} \\ h_{z} \\ s_{s} \end{pmatrix}$	(165.0) $\begin{array}{c} v_{s} \\ u_{s} \\ h_{s} \\ s_{s} \end{array}$	$\begin{pmatrix} 6 \\ u_s \\ h_s \\ s_r \end{pmatrix}$	(151.8) $\begin{array}{c} v_{*} \\ s_{*} \\ s_{*} \end{array}$	p/[bear] (7,/[°C])	
* See footnote on p. 6.	$\begin{array}{cccc} & v_{s} & 0.0274 \\ 70 & u_{s}^{s} & 2581 \\ (285.8) & s_{s}^{s} & 5814 \\ & s_{s} & 5814 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 50 \\ (263.9) \\ s_{\mu} \\ s_{\mu} \\ s_{\mu} \\ s_{\mu} \\ 5.973 \\ s_{\mu} \\ 5.973 \end{array}$	$\begin{array}{c} 40 \\ (250.3) \\ s_{\pi} \\ s_{\pi} \\ \end{array} \begin{array}{c} v_{x} \\ 2602 \\ s_{\pi} \\ 6.070 \\ \end{array}$	$\begin{array}{ccccc} 30 & u_{\pi} & 0.0666 \\ 30 & u_{\pi} & 2603 \\ (233.8) & h_{\pi} & 2803 \\ s_{\pi} & 6.186 \end{array}$	$\begin{array}{cccccccc} & v_{\rm F} & 0.0996 \\ 20 & u_{\rm F} & 2600 \\ \lambda_{\rm F} & 2799 \\ s_{\rm F} & 6.340 \end{array}$	$\begin{array}{c} 15 \\ 198.3 \\ 198.3 \\ s_{\rm b} \end{array} \qquad \begin{array}{c} v_{\rm g} \\ 0.1317 \\ h_{\rm g} \\ 2595 \\ s_{\rm g} \\ 6.445 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9 $v_{\rm g}$ 0.2149 (175.4) $h_{\rm g}$ 2581 $s_{\rm g}$ 6.623	$\begin{array}{c} 8 \\ 8 \\ (170.4) \\ 4 \\ s_{\pi} \\ s_{\pi} \\ s_{\pi} \\ 6.663 \end{array} $	$\begin{array}{cccc} 7 & v_{s} & 0.2728 \\ r_{s} & 2573 \\ r_{s} & 2764 \\ s_{s} & 6.709 \end{array}$	$\begin{array}{cccc} 6 & v_{\rm g} & 0.3156 \\ 158.8) & h_{\rm g}^{\rm g} & 2568 \\ s_{\rm g} & 6.761 \end{array}$	$\begin{array}{cccc} & & v_{\pm} & 0.3748 \\ & S & & u_{\pm} & 2562 \\ & & h_{\pm} & 2749 \\ & & s_{\pm} & 6.822 \end{array}$	/[bar] (7,/[°C])	
* See footnote on p. 6.	$\begin{array}{ccccccc} 70 & v_s & 0.0274 & v_s (m^3) \\ (285.8) & h_s & 2772 & u_s (LL) \\ s_s & 5.814 & s_s (LL) \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\frac{p/[bar]}{(T,l^{c}C)} \qquad \frac{T}{[^{c}C]}$	
* See footnote on p. 6.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\frac{p(\text{lbar})}{(T, l^{\text{rc}})} \qquad \frac{T}{[\text{rc}]} 200$	
* See footnote on p. 6.	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	p/[ber] r (7,/[°C]) [°C] 200 250	
[*] See footnote on p. 6.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\frac{p/[ber]}{(T,/[^{c}C])}$ $\frac{T}{[^{c}C]}$ 200 250 300	
* See footnote on p. 6.	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	p/[bar] (T,/[°C]) T [°C] 200 250 300 350	
* See footnote on p. 6.	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	p/[bar] T 200 250 300 350 400	
* See footnote on p. 6.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\frac{p(\text{lbear}]}{(T, l^{\text{PC}})} \frac{T}{[\text{CC}]} 200 250 300 350 400 450$	Supe
* See footnote on p. 6.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	p/[ber] T 200 250 300 350 400 450 500	Superheated

\$

Note: linear interpolation is not accurate near the critical point.

* See footno	221.2 (374.15)	220 (373.7)	210 (369.8)	200 (365.7)	190 (361.4)	180 (357.0)	170 (352.3)	160 (347.3)	150 (342.1)	140 (336.6)	130 (330.8)	120 (324.6)	110 (318.0)	(3110)	90 (303.3)	80 (295.0)	p/[bar] (7,/[°C])	Superheate
teon p. 6.		v, 0.00368 h, 2178 s _e 4.552	v, 0.00498 h, 2336 s _∎ 4,803	v, 0.00585 h, 2411 s _s 4.928	v, 0.00668 h, 2466 s_i 5.027	p _s 0.00751 h, 2510 s _t 5.108	v, 0.00838 h, 2548 s ₁ 5.181	v 0.00932 h, 2582 s ₈ 5.248	v, 0.01035 h, 2611 s _e 5.312	v, 0.01149 h 2638 s 5.373	<i>b</i> 0.01278 <i>h</i> 2662 s 5.433	v, 0.01426 h, 2685 s _a 5.493	v, 0.01598 h, 2705 s, 5.553	v, 0.01802 h, 2725 s, 5.615	v, 0.02048 h, 2743 s _∎ 5.679	v, 0.02352 h, 2758 s, 5.744		d Steam*
	v/10 ⁻² s	p/10- x s	₩ #	s/[kJ/k] h/[kJ/k]	t/10 ⁻² s	v/10 ^{−2} k	v/10 ⁻²	v/10 ⁻² h s	p/10 ⁻²	v/10 ⁻² s	v/10 ⁻²	5 - 01/2 5	p/10 ⁻² h	c/10 ⁻² h	r/10-2	v/10 ⁻² 5	r TCJ r	
	0.163 1637 3.708			ξ K] [1] [1] [1] [1] [1] [1] [1] [1] [1] [1				0.976 2617 5.304	1.146 2693 5.443	1,321 2753 5.559	1.509 2804 5.664	1.719 2849 5.762	1.960 2889 5.856	2.241 2926 5.947	2,578 2959 6.039	2.994 2990 6.133	350	
	0.351 2139 4.490	0.450 2300 4.725	0.650 2500 5.050	0.768 2605 5.228	0.882 2674 5.348	0.997 2729 5.449	1.117 2778 5.541	1.248 2821 5.626	1.391 2861 5.707	1.548 2896 5.784	1.726 2929 5.862	1.931 2960 5.937	2,169 2989 6.014	2.453 3017 6.091	2.794 3042 6.171	3.220 3067 6.255	375	
	0.816 2733 5.398	0.825 2738 5.409	0.908 2781 5.484	0.995 2819 5.556	1.089 2855 5.625	1.191 2888 5.691	1,303 2920 5.756	1.427 2949 5.820	1.566 2977 5.883	1.722 3003 5.946	1.901 3028 6.011	2,107 3052 6.076	2.350 3075 6.143	2.639 3097 6.213	2.991 3118 6.286	3,428 3139 6,364	400	
	0.978 2896 5.638	0.987 2900 5.645	1.064 2928 5.699	1.147 2955 5.753	1,238 2980 5.807	1,338 3004 5.861	1.449 3028 5.914	1.573 3051 5.968	1.714 3073 6.023	1.872 3093 6.079	2.053 3114 6.136	2.265 3134 6.195	2.514 3153 6.257	2.812 3172 6.321	3.173 3189 6.390	3.625 3207 6.463	425	
	1.103 3017 5.807	1.111 3020 5.813	1.187 3041 5.859	1.270 3062 5.904	1.362 3082 5.950	1,463 3102 5,997	1.576 3121 6.044	1.702 3139 6.093	1.844 3157 6.142	2.006 3175 6.193	2.193 3192 6.246	2,410 3209 6,301	2.666 3225 6.358	2.972 3241 6.419	3.346 3256 6.484	3.812 3272 6.555	450	
	6.064 1.303	1.312 3210 6.068	1,390 3225 6,105	1.477 3239 6.142	1.572 3254 6.180	1.678 3268 6.219	1.796 3281 6.260	1.928 3295 6.301	2.078 3309 6.345	2,250 3322 6,390	2.447 3335 6.437	2.677 3348 6.487	2.949 3360 6.539	3.275 3373 6.596	3.673 3385 6.657	4.170 3398 6.723	SOO	
	1.622 3518 6.441	1,632 3519 6,444	1.719 3528 6.474	1.815 3537 6.505	1.921 3546 6.536	2.039 3555 6.569	2.171 3564 6.603	2.319 3573 6.639	2.487 3581 6.677	2.679 3590 6.716	2.901 3599 6.758	3.159 3607 6.802	3.465 3616 6.850	3.831 3624 6.902	4.279 3633 6.958	4,839 3641 7.019	600	
	1.895 3792 6.739	1.906 3793 6.742	2.003 3799 6.768	2.110 3806 6.796	2.228 3812 6.825	2.359 3818 6.855	2.506 3825 6.886	2.670 3831 6.919	2.857 3837 6.954	3.071 3843 6.991	3.318 3850 7.030	3.605 3856 7.072	3.945 3862 7.117	4.353 3868 7.166	4.852 3874 7.220	5.476 3881 7.279	700	
				2		.				-							;	
																1		
* See foo	1000	900	800	750	700	650	600	550	500	450	400	350	300	275	250	225	[bar]	
* See footnote on p. 6.	$1000 \begin{bmatrix} r/10^{-2} \\ h \\ s \end{bmatrix}$	900 $\frac{v}{3}$	$800 k^{1/10^{-2}}$	750 $\frac{b^{1/2}}{h}$	$\frac{b/10^{-2}}{s}$	$650 \begin{bmatrix} v/10^{-2} \\ h \\ s \end{bmatrix}$	600 $\frac{i/10^{-2}}{5}$	550 <i>k</i> /10 ⁻²	500 h	450 $\frac{b}{5}$	$\frac{t}{400}$ $\frac{t}{h}$	$350 \qquad \begin{vmatrix} r/10 \\ h \\ s \end{vmatrix}$	$\frac{r}{h}^{10^{-2}}$	275 k	250 h/10 ⁻²	225 %/LU ⁻² [m ³ /kg] %/LU/kg] %/KJ/kg/K]	p T [bar] ["C]	
*See footnote on p. 6.	$\begin{array}{c cccc} 1000 & \frac{r}{h} & 0.131 \\ s & 1.552 \\ s & 3.394 \end{array}$	900 $\frac{v/10^{-2}}{5}$ 0.133 3.418	$\begin{array}{c c} 800 \\ k \\ s \\ 3.444 \end{array} $	750 $\frac{e/10^{-2}}{h}$ 1559 3.459	700 $\frac{p/10^{-2}}{5}$ 0.138 3.473	$\begin{array}{c cccc} & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & s & & & &$	$\begin{array}{c c} 600 \\ h\\ 5 \\ 3.506 \\ \end{array} $	$\begin{array}{c} t/10^{-2} & 0.143 \\ 550 & h & 1572 \\ s & 3.525 \end{array}$	500 h 1577 3.544	$\begin{array}{ccc} & & & & \\ 450 & h & & & \\ & s & & & \\ & & & & 3.565 \end{array}$	$\begin{array}{c} t/10^{-2} \\ 400 \\ s \\ 3.588 \end{array}$	350 t/10 ² 0.152 s 3.614	$\begin{array}{ccc} r_{1}^{\prime}10^{-2} & 0.155\\ 300 & h & 1610\\ s & 3.645 \end{array}$	$\begin{array}{cccc} r/10 & 2 & 0.158 \\ r/10 & 1617 \\ r/10 & r/10 \\ r/10 & 1617 \\ r$	$\begin{array}{c} r/10^{-2} & 0.160 \\ h & 1625 \\ s & 3.682 \end{array}$	225 b/[LJ/kg] 0.163 b/[LJ/kg] 1635 s/[KJ/kgK] 3.704	$\frac{p}{[bar]}$ $\frac{T}{[C]}$ 350	
* See footnote on p. 6.	$\begin{array}{c ccccc} r/10^{-2} & 0.131 & 0.138 \\ h & 1552 & 1674 \\ s & 3.394 & 3.584 \end{array}$	900 $\frac{v}{10^{-2}}$ 0.133 0.140 5 3.3.418 3.612	$\begin{array}{c cccc} 800 & \frac{v}{10} & 0.136 & 0.143 \\ h & 1557 & 1684 \\ s & 3.444 & 3.642 \end{array}$	750 $\frac{r/10^{-2}}{s}$ 0.137 0.145 3.459 1687 3.459 3.659	700 $\frac{v}{10}^{-2}$ 0.138 0.146 s 3.473 3.678	$\begin{array}{c ccccc} & & & & & & \\ & & & & & & \\ 650 & h & & & & \\ s & & & & & 3.489 & 3.697 \end{array}$	$\begin{array}{c ccccc} 600 & \frac{17}{10} & 0.141 & 0.151 \\ 5 & 1568 & 1702 \\ 5 & 3.506 & 3.718 \end{array}$	$\begin{array}{ccccc} & t_{1}/10^{-2} & 0.143 & 0.153 \\ & h & 1572 & 1709 \\ & s & 3.525 & 3.742 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccc} v/10^{-2} & 0.146 & 0.160 \\ h & 1583 & 1729 \\ s & 3.565 & 3.797 \end{array}$	400 $\frac{v}{10^{-2}}$ 0.149 0.164 $\frac{h}{s}$ 3.588 3.832	$\begin{array}{cccccc} 350 & \frac{r}{10} & 2 & 0.152 & 0.171 \\ 3 & & 1599 & 1762 \\ 3 & & 3.614 & 3.875 \end{array}$	$\begin{array}{ccccc} 300 & h^{2}/10^{-2} & 0.155 & 0.180 \\ & & & 1610 & 1791 \\ s & & 3.645 & 3.933 \end{array}$	275 k ¹ /10 ⁻² 0.158 0.187 k 1617 1814 s 3.662 3.985	$\begin{array}{ccccc} r/10^{-2} & 0.160 & 0.198 \\ 250 & h & 1625 & 1850 \\ s & 3.682 & 4.026 \end{array}$	225 <i>s</i> /10 ⁻² [m ³ /kg] 0.163 0.249 <i>i</i> /[k1/kg] 1635 1980 <i>s</i> /[k1/kg K] 3.704 4.470	n T 350 375 [bar] [°C] 350 375	
* See footnote on p. 6.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	900 $\frac{v/10^{-2}}{s}$ 0.133 0.140 0.148 1554 1678 1805 3 3.418 3.612 3.805	$\begin{array}{c ccccc} & v/10^{-2} & 0.136 & 0.143 & 0.152 \\ & & 1557 & 1684 & 1815 \\ s & & 3.444 & 3.642 & 3.842 \end{array}$	750 $\frac{t}{10}$ t^{-2} 0.137 0.145 0.154 1559 1687 1821 3 3.459 3.659 3.863	700 $\frac{v}{10}^{-2}$ 0.138 0.146 0.157 760 $\frac{h}{5}$ 3.473 3.678 3.886	$\begin{array}{c ccccc} & & & & & \\ & & & & & \\ 650 & h & & & & \\ & s & & & & & \\ & s & & & & &$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccc} 450 & \frac{\nu}{10} & 0.145 & 0.160 & 0.181 \\ & h & 1583 & 1729 & 1901 \\ s & 3.565 & 3.797 & 4.056 \end{array}$	$\begin{array}{ccccccc} & & & & & & \\ & & & & & & \\ 400 & h & & & & & \\ & s & & & & & & \\ & s & & & &$	$\begin{array}{ccccccc} x/10^{-2} & 0.152 & 0.171 & 0.211 \\ 3 & 1599 & 1762 & 1992 \\ 3 & 3.614 & 3.875 & 4.219 \end{array}$	$\begin{array}{cccccc} 300 & h^{1/10^{-2}} & 0.155 & 0.180 & 0.282 \\ h & 1610 & 1791 & 2157 \\ s & 3.645 & 3.933 & 4.482 \end{array}$	275 h 0.158 0.187 0.419 s 3.662 3.985 4.828	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	225 h[[kJ]kg] 0.163 0.249 0.786 h[[kJ]kg] 1635 1980 2716 s/[kJ]kg K] 3.704 4.470 5.369	n T 350 375 400	
* See footnote on p. 6.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	900 $\frac{w}{10^{-2}}$ 0.133 0.140 0.148 0.158 3.418 3.612 3.805 3.991	$\begin{array}{c ccccc} 800 \\ s \\ s \\ \end{array} \begin{array}{c ccccccc} n/10^{-2} \\ s \\ s \\ 3,444 \\ 3,642 \\ 3,642 \\ 3,842 \\ 4.037 \\ \end{array} \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccc} & & & & & & \\ & & & & & & \\ 450 & h & & & & & \\ & s & & & & & \\ & s & & & &$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	225 h[[L1/kg] 0.163 0.249 0.786 0.95] h[[L1/kg] 1635 1980 2716 2885 s/[L1/kgK] 3.704 4.470 5.369 5.616	n T 350 375 400 425	
* See footnote on p. 6.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	900 $\frac{w}{10^{-2}}$ 0.133 0.140 0.148 0.158 0.169 3 3.418 3.612 3.805 3.991 4.179	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	750 h 137 0.145 0.154 0.167 0.183 s 3.459 1.687 1.821 1.958 2107 s 3.459 3.659 3.863 4.064 4.272	700 $\frac{v}{10^{-2}}$ 0.138 0.146 0.157 0.171 0.189 s 3.473 3.678 3.886 4.093 4.312	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	tr/10 ⁻² 0.144 0.156 0.173 0.201 0.249 500 h 1577 1717 1879 2064 2288 3.544 3.768 4.009 4.279 4.594	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	350 k 10 ⁻² 0.152 0.171 0.211 0.343 0.496 3 3.614 3.875 4.219 4.776 5.197	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	250 h 1625 1850 2880 2807 2951 3.682 4.026 5.142 5.474 5.677	225 h[[k1/kg] 1635 1980 2716 2885 3009 s/[k1/kg] 3.704 4.470 5.369 5.616 5.790	n T 350 375 400 425 450	
* See footnote on p. 6.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	900 $\frac{v}{h}^{10^{-2}}$ 0.133 0.140 0.148 0.158 0.169 0.202 3.418 3.612 3.805 3.991 4.179 4.563	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	750 h 1559 1687 1821 1958 2107 2431 s 3.459 3.659 3.863 4.064 4.272 4.705	700 $\frac{p}{10}^{-2}$ 0.138 0.146 0.157 0.171 0.189 0.247 5 3.473 3.678 3.886 4.093 4.312 4.769	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	tr/10 ⁻² 0.143 0.153 0.168 0.190 0.224 0.334 550 h 1572 1709 1862 2030 2227 2641 s 3.525 3.742 3.971 4.218 4.494 5.047	500 h 0.144 0.156 0.173 0.201 0.249 0.388 500 h 1577 1717 1879 2064 2288 2722 3.544 3.768 4.009 4.279 4.594 5.176	450 h 10 ⁻² 0.146 0.160 0.181 0.219 0.291 0.463 s 3.565 3.797 4.056 4.368 4.740 5.320	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	350 k 1/10 ² 0.152 0.171 0.211 0.343 0.496 0.693 350 k 1599 1762 1992 2.375 2.673 2.998 3.614 3.875 4.219 4.776 5.197 5.633	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	225 h/[L1/kg] 163 0.249 0.786 0.951 1.076 1.275 h/[L1/kg] 1635 1980 2716 2885 3009 3203 s/[KJ/kg K] 3.704 4.470 5.369 5.616 5.790 6.050	n T 350 375 400 425 450 500	
* See footnote on p. 6.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	900 h 1554 1678 1805 1932 2066 2353 2916 3 3.418 3.612 3.805 3.991 4.179 4.563 5.248	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	750 h 1559 1687 1821 1958 2107 2431 3021 s 3.459 3.659 3.863 4.064 4.272 4.705 5.425	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	tr/10 ⁻¹ 0.144 0.156 0.173 0.201 0.249 0.388 0.611 500 h 1577 1717 1879 2064 2288 2722 3249 500 h 3.544 3.768 4.009 4.279 4.594 5.176 5.821	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	275 h 1617 1814 2382 2718 2890 3125 x 3.662 3.985 4.828 5.320 5.562 5.878 6.296	250 h 1625 1850 2580 2807 2951 1.113 1.412 3.682 4.026 5.142 5.474 5.677 5.962 6.361	v/10 ⁻² [m ³ /kg] 0.163 0.249 0.786 0.951 1.076 1.275 1.591 225 h/[[k,1/kg] 1635 1980 2716 2885 3009 3203 3514 s/[k,1/kg] 3.704 4.470 5.369 5.616 5.790 6.050 6.430	n T 350 375 400 425 450 500 600	Supe
* See footnote on p. 6.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	900 $\frac{v}{h}^{10^{-2}}$ 0.133 0.140 0.148 0.158 0.169 0.202 0.296 0.396 3.418 3.612 3.805 3.991 4.179 4.563 5.248 5.746	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	750 h 137 0.145 0.154 0.167 0.183 0.231 0.365 0.486 x 3.459 1.687 1.821 1.958 2.107 2.431 3021 3.456 x 3.459 3.659 3.863 4.064 4.272 4.705 5.425 5.899	700 h 10 ⁻² 0.138 0.146 0.157 0.171 0.189 0.247 0.397 0.526 3 3.473 3.678 3.886 4.093 4.312 4.769 5.494 5.955	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	tr/10 2 0.152 0.171 0.211 0.343 0.496 0.693 0.952 1.152 350 h 1599 1762 1992 2.375 2673 2998 3397 3709 3 3.614 3.875 4.219 4.776 5.197 5.633 6.120 6.459	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	c/10 ⁻² 0.160 0.198 0.601 0.789 0.917 1.113 1.412 1.662 250 h 1625 1850 2580 2807 2951 3165 3491 3774 3 3.682 4.026 5.142 5.474 5.677 5.962 6.361 6.667	v/10 ⁻² [m ³ /kg] 0.163 0.249 0.786 0.951 1.076 1.275 1.591 1.861 225 h/[k1/kg] 1635 1980 2716 2885 3009 3203 3514 3790 s/[k1/kg]K] 3.704 4.470 5.369 5.616 5.790 6.050 6.430 6.729	n T 350 375 400 425 450 500 600 700	Supercritical

Enthalpy Entropy Chart for Steam

(using data from NEL Steam Tables 1964 and other formulations: for exercises only)





2001 ASHRAE Fundamentals Handbook (SI)

Table 2 Thermodynamic Properties of Moist Air at Standard Atmospheric Pressure, 101.325 kPa (Continued)

												Condensed Water		
Temp.	Humidity , Ratio,	Specific Volume, m ³ /kg (drv alr)			Specific Enthalpy, kJ/kg (dry air)			Specific Entropy, kJ/(kg·K) (dry air)			Specific Enthalpy, k 1/kg	Specific Entropy, kI/(kg·K)	Vapor Pressure, kPa	Temp., °C
°C	kg(w)/kg(da) W.	 	y _{ar}	 V _S	h _{da}	h _{da}	h _s	s _{da}	S _{ds}	S _S	h _w	5 _W	P ₅	ť
14 15 16 17 18	0.010012 0.010692 0.011413 0.012178 0.012989 0.012989	0.8132 0.8160 0.8168 0.8217 0.8245 0.8274	0.0131 0.0140 0.0150 0.0160 0.0172 0.0184	0.8262 0.8300 0.8338 0.8377 0.8417 0.8457	14.084 15.090 16.096 17.102 18.108 19.114	25.286 27.023 28.867 30.824 32.900 35.101	39.370 42.113 44.963 47.926 51.008 54.216	0.0503 0.0538 0.0573 0.0607 0.0642 0.0677	0.0927 0.0987 0.1051 0.1119 0.1190 0.1266	0.1430 0.1525 0.1624 0.1726 0.1832 0.1942	58.88 63.07 67.26 71.44 75.63 79.81	0.2099 0.2244 0.2389 0.2534 0.2678 0.2821	1.5987 1.7055 1.8185 1.9380 2.0643 2.1979	14 15 16 17 18 19
20 21 22 23 24 25 26 27 28	0.014758 0.015721 0.016741 0.017821 0.018963 0.020170 0.021448 0.022798 0.024226	0.8302 0.8330 0.8359 0.8387 0.8416 0.8444 0.8472 0.8501 0.8501 0.8529	0.0196 0.0210 0.0224 0.0256 0.0273 0.0291 0.0311 0.0331	0.8498 0.8540 0.8583 0.8627 0.8671 0.8717 0.8764 0.8811 0.8860	20.121 21.127 22.133 23.140 24.146 25.153 26.159 27.165 28.172	37.434 39.908 42.527 45.301 48.239 51.347 54.638 58.120 61.804	57.555 61.035 64.660 68.440 72.385 76.500 80.798 85.285 89.976	0.0711 0.0745 0.0779 0.0813 0.0847 0.0881 0.0915 0.0948 0.0982	0.1346 0.1430 0.1519 0.1613 0.1712 0.1817 0.1927 0.2044 0.2166	0.2057 0.2175 0.2298 0.2426 0.2559 0.2698 0.2842 0.2992 0.3148	84.00 88.18 92.36 96.55 100.73 104.91 109.09 113.27 117.45	0.2965 0.3107 0.3249 0.3390 0.3531 0.3672 0.3812 0.3951 0.4090	2.3389 2.4878 2.6448 2.8105 2.9852 3.1693 3.3633 3.5674 3.7823	20 21 22 23 24 25 26 27 28 28
29 30 31 32 33 34 35 36 37 38	0.025735 0.027329 0.029014 0.030793 0.032674 0.034660 0.036756 0.038971 0.041309 0.043778	0.8558 0.8586 0.8614 0.8643 0.8671 0.8700 0.8728 0.8756 0.8785 0.8813	0.0353 0.0376 0.0400 0.0426 0.0454 0.0483 0.0514 0.0581 0.0581 0.0618	0.8910 0.8962 0.9015 0.9069 0.9125 0.9183 0.9242 0.9303 0.9366 0.9431 0.948	29.179 30.185 31.192 32.198 33.205 34.212 35.219 36.226 37.233 38.239 39.246	65.699 69.820 74.177 78.780 83.652 88.799 94.236 99.983 106.058 112.474 119.258	94.878 100.006 105.369 110.979 116.857 123.011 129.455 136.209 143.290 150.713 158.504	0.1015 0.1048 0.1082 0.1115 0.1148 0.1213 0.1246 0.1278 0.1311 0.1343	0.2296 0.2432 0.2576 0.2728 0.3056 0.3233 0.3420 0.3617 0.3824 0.4043	0.3311 0.3481 0.3658 0.3842 0.4035 0.4236 0.4446 0.4666 0.4895 0.5135 0.5386	121.63 125.81 129.99 134.17 138.35 142.53 146.71 150.89 155.07 159.25 163.43	0.4229 0.4367 0.4505 0.4642 0.4779 0.4915 0.5051 0.5186 0.5321 0.5456 0.5590	4.0084 4.2462 4.4961 4.7586 5.0345 5.3242 5.6280 5.9468 6.2812 6.6315 6.9988	29 30 31 32 33 34 35 36 37 38 39
39 40 41 42 43 44 45 46 47 48 49	0.046386 0.049141 0.052049 0.055119 0.058365 0.061791 0.065411 0.069239 0.073282 0.077556 0.09277	0.8842 0.8870 0.8898 0.8927 0.8955 0.8983 0.9012 0.9040 0.9069 0.9097 0.9125	0.0637 0.0698 0.0741 0.0788 0.0837 0.0888 0.0943 0.1002 0.1063 0.1129 0.1198	0.9498 0.9568 0.9640 0.9714 0.9792 0.9872 0.9955 1.0042 1.0132 1.0226 1.0323	40.253 41.261 42.268 43.275 44.282 45.289 46.296 47.304 48.311 49.319	126.430 134.005 142.007 150.475 159.417 168.874 178.882 189.455 200.644 212.485	166.683 175.265 184.275 193.749 203.699 214.164 225.179 236.759 248.955 261.803	0.1375 0.1407 0.1439 0.1471 0.1503 0.1535 0.1566 0.1598 0.1629 0.1661	0.4273 0.4516 0.4771 0.5041 0.5325 0.5624 0.5940 0.6273 0.6624 0.6994	0.5649 0.5923 0.6211 0.6512 0.6828 0.7159 0.7507 0.7871 0.8253 0.8655	167.61 171.79 175.97 180.15 184.33 188.51 192.69 196.88 201.06 205.24	0.5724 0.5857 0.5990 0.6122 0.6254 0.6386 0.6517 0.6648 0.6778 0.6908	7.3838 7.7866 8.2081 8.6495 9.1110 9.5935 10.0982 10.6250 11.1754 11.7502	40 41 42 43 44 45 46 47 48 49
49 50 51 52 53 54 55 56 57 58 58	0.086858 0.091918 0.097272 0.102948 0.108954 0.115321 0.122077 0.129243 0.136851 0.140422	0.9123 0.9154 0.9182 0.9211 0.9239 0.9267 0.9296 0.9324 0.9353 0.9381 0.9409	0.1272 0.1350 0.1433 0.1521 0.1614 0.1713 0.1819 0.1932 0.2051 0.2179	1.0425 1.0532 1.0643 1.0760 1.0882 1.1009 1.1143 1.1284 1.1432 1.1588	50.326 51.334 52.341 53.349 54.357 55.365 56.373 57.381 58.389 59.397	225.019 238.290 252.340 267,247 283.031 299.772 317.549 336.417 356.461 377.788	275.345 289.624 304.682 320.596 337.388 355.137 373.922 393.798 414.850 437.185	0.1692 0.1723 0.1754 0.1785 0.1816 0.1847 0.1877 0.1908 0.1938 0.1969	0.7385 0.7798 0.8234 0.8695 0.9182 0.9698 1.0243 1.0820 1.1432 1.2081	0.9077 0.9521 0.9988 1.0480 1.0998 1.1544 1.2120 1.2728 1.3370 1.4050	209.42 213.60 217.78 221.97 226.15 230.33 234.52 238.70 242.88 247.07	0.7038 0.7167 0.7296 0.7424 0.7552 0.7680 0.7807 0.7934 0.8061 0.8187	12.3503 12.9764 13.6293 14.3108 15.0205 15.7601 16.5311 17.3337 18.1691 19.0393	50 51 52 53 54 55 56 57 58 59
60 61 62 63 64 65 66 67 68 69	0.15354 0.16259 0.17244 0.18284 0.19393 0.20579 0.21848 0.23207 0.24664 0.26231	0.9438 0.9466 0.9494 0.9523 0.9551 0.9580 0.9608 0.9665 0.9665 0.9663	0.2315 0.2460 0.2614 0.2780 0.2957 0.3147 0.3350 0.3568 0.3803 0.4055	1.1752 1.1926 1.2109 1.2303 1.2508 1.2726 1.2958 1.3204 1.3467 1.3749	60.405 61.413 62.421 63.429 64.438 65.446 66.455 67.463 68.472 69.481	400.458 424.624 450.377 477.837 507.177 538.548 572.116 608.103 646.724 688.261	460.863 486.036 512.798 541.266 571.615 603.995 638.571 675.566 715.196 757.742	0.1999 0.2029 0.2059 0.2089 0.2119 0.2149 0.2179 0.2209 0.2238 0.2268	1.2769 1.3500 1.4278 1.5104 1.5985 1.6925 1.7927 1.8999 2.0147 2.1378	1.4768 1.5530 1.6337 1.7194 1.8105 1.9074 2.0106 2.1208 2.2385 2.3646	251.25 255.44 259.62 263.81 268.00 272.18 276.37 280.56 284.75 288.94	0.8313 0.8438 0.8563 0.8688 0.8812 0.8936 0.9060 0.9183 0.9306 0.9429	19.9439 20.8858 21.8651 22.8826 23.9405 25.0397 26.1810 27.3664 28.5967 29.8741	60 61 63 64 65 66 67 68 69
70 71 72 73 74 75 76 77 78 79	0.27916 0.29734 0.31698 0.33824 0.36130 0.38641 0.41377 0.44372 0.47663 0.51284	0.9721 0.9750 0.9778 0.9807 0.9835 0.9863 0.9892 0.9920 0.9948 0.9977	0.4328 0.4622 0.4941 0.5287 0.5662 0.6072 0.6519 0.7010 0.7550 0.8145	1.4049 1.4372 1.4719 1.5093 1.5497 1.5935 1.6411 1.6930 1.7498 1.8121	70.489 71.498 72.507 73.516 74.525 75.535 76.543 77.553 78.562 79.572	732.959 781.208 833.335 889.807 951.077 1017.841 1090.628 1170.328 1257.921 1354.347	803.448 852.706 905.842 963.323 1025.603 1093.375 1167.172 1247.881 1336.483 1433.918	0.2297 0.2327 0.2356 0.2385 0.2414 0.2443 0.2472 0.2501 0.2530 0.2559	2.2699 2.4122 2.5655 2.7311 2.9104 3.1052 3.3171 3.5486 3.8023 4.0810	2,4996 2,6448 2,8010 2,9696 3,1518 3,3496 3,5644 3,7987 4,0553 4,3368	293.13 297.32 301.51 305.70 309.89 314.08 318.28 322.47 326.67 330.86	0.9551 0.9673 0.9794 0.9916 1.0037 1.0157 1.0278 1.0278 1.0398 1.0517 1.0636	31.1986 32.5734 33.9983 35.4759 37.0063 38.5940 40.2369 41.9388 43.7020 45.5248	70 71 72 73 74 75 76 77 78 79
80 81 82 83 84 85 86 87 88 87 88 89	0.55295 0.59751 0.64724 0.70311 0.76624 0.83812 0.92062 1.01611 1.12800 1.26064 1.42031	1.0005 1.0034 1.0062 1.0090 1.0119 1.0147 1.0175 1.0204 1.0232 1.0261	0.8805 0.9539 1.0360 1.1283 1.2328 1.3518 1.4887 1.6473 1.8333 2.0540 2.3199	1.8810 1.9572 2.0422 2.1373 2.2446 2.3666 2.5062 2.6676 2.8565 3.0800 3.3488	80.581 81.591 82.600 83.610 84.620 85.630 86.640 87.650 88.661 89.671 90.681	1461.200 1579.961 1712.547 1861.548 2029.983 2221.806 2442.036 2697.016 2995.890 3350.254 3776.918	1541.781 1661.552 1795.148 1945.158 2114.603 2507.436 2528.677 2784.666 3084.551 3439.925 3867.599	0.2587 0.2616 0.2644 0.2673 0.2701 0.2729 0.2757 0.2785 0.2813 0.2841 0.2869	4.3890 4.7305 5.1108 5.5372 6.0181 6.5644 7.1901 7.9128 8.7580 9.7577 10.9586	4.6477 4.9921 5.3753 5.8045 6.2882 6.8373 7.4658 8.1914 9.0393 10.0419 11.2455	335.06 339.25 343.45 347.65 351.85 356.05 360.25 364.45 368.65 372.86 377.06	1.0755 1.0874 1.0993 1.1111 1.1228 1.1346 1.1463 1.1580 1.1696 1.1812 1.1928	47.4135 49.3670 51.3860 53.4746 55.6337 57.8658 60.1727 62.5544 65.0166 67.5581 70.1817	80 81 82 83 84 85 86 87 88 87 88 89 90

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