$\frac{\text { UNIVERSITY }}{\text { JOHANNESBURG }}$

| PROGRAM | BACHELOR OF ENGINEERING TECHNOLOGY ENGINEERING : CIVIL |
| :---: | :---: |
| SUBJECT | GEOTECHNICAL ENGINEERING 2B |
| CODE | GTECIB2 |
| DATE | NOVEMBER EXAMINATION 23 NOVEMBER 2019 |
| DURATION | (X-PAPER) 08:30-11:30 |
| FULL MARKS | 100 |
| TOTAL MARKS | 100 |
| EXAMINER | PROF G C FANOURAKIS |
| MODERATOR | DR B A HARRISON |
| NUMBER OF PAGES | 3 PAGES AND 5 ANNEXURES |
| INSTRUCTIONS | STUDENTS MAY BRING AN A4 SIZE SHEET OF PAPER |
|  | INTO THE EXAMINATION VENUE. THIS SHEET MAY |
|  | CONTAIN EQUATIONS / FORMULAE WHICH HAVE |
|  | BEEN ORIGINALLY HANDWRITTEN (NOT |
|  | PHOTOCOPIED) ON BOTH SIDES. |
|  | PROGRAMMABLE CALCULATORS ARE PERMITTED (ONLY ONE PER STUDENT). |
|  | WHERE RELEVANT, TAKE ACCELERATION DUE TO GRAVITY AS $10 \mathrm{~m} / \mathrm{s}^{2}$. |
| REQUIREMENTS | GRAPH PAPER |

## QUESTION 1

Briefly discuss how soil particle size distribution, shape and texture affect the permeability of a soil.

## QUESTION 2

A flow net through an earth dam is shown in Figure 1 (attached).
2.1 If the dam is 100 m long and the coefficient of permeability ( k ) is 7 x $10^{-7} \mathrm{~m} / \mathrm{sec}$, calculate the total seepage through the dam in $\mathrm{m}^{3} / \mathrm{sec}$.
2.2 Determine the critrical hydraulic gradient $\left(i_{c}\right)$ if the soil has a dry density of $1800 \mathrm{~kg} / \mathrm{m}^{3}$ and a saturated moisture content of $20 \%$.
2.3 Determine the water level "h" in the stand pipe shown.

## QUESTION 3

A lake comprises 4 m of water overlying 5 m of clay. The clay has a unit weight $(\gamma)$ of $19 \mathrm{kN} / \mathrm{m}^{3}$.
3.1 Plot the variation in total stress, pore water pressure and effective stress with depth.
3.2 What would be the value of the pore water pressures at the top and bottom of the clay layer, immediately after a drop in the water table of 2 m ?

## QUESTION 4

The results of a consolidated undrained triaxial test carried out on a soil sample are given below. Assuming the cross-sectional area at failure of each specimen to have been $1414 \mathrm{~mm}^{2}$, determine the total and effective shear strength parameters of this soil.

| Specimen No. | Cell Pressure (kPa) | Axial Load at <br> Failure (N) | Pore Water <br> Pressure (kPa) |
| :--- | :--- | :--- | :--- |
| 1 | 67 | 312 | 20 |
| 2 | 167 | 469 | 80 |
| 3 | 267 | 654 | 135 |

## QUESTION 5

Determine the magnitude of the resultant thrust, per unit length, acting on the gabion wall, shown in Figure 2 (attached).

## QUESTION 6

Determine the factor of safety for the slope shown in Figure 3 (attached).

## QUESTION 7

Figure 4 shows the plan of a rectangular foundation which transmits a uniform contact pressure of 240 kPa . Using Steinbrenner's method, and the chart provided, determine the vertical stress caused by this loading at a depth of 5 m below A.

## QUESTION 8

The results of a laboratory consolidation test, on a clay, are given below.

| Pressure (kPa) | Void Ratio (e) |
| :--- | :--- |
| 23,94 | 1,112 |
| 47,88 | 1,105 |
| 95,76 | 1,080 |
| 191,52 | 0,985 |
| 383,04 | 0,850 |
| 766,08 | 0,731 |

8.1 Plot the $\mathrm{e}-\log \mathrm{P}$ curve on Figure 5 (attached).
8.2 Determine the preconsolidation pressure.

## PLEASE HAND IN FIGURE 5 WITH YOUR SCRIPT



Figure 1


Figure 2



Not to Scale

Figure 4
Figure 5

| b/l | 0 | 0,1 | 0,2 | 1/3 | 0,4 | 0,5 | 2/3 | 1 | 1,5 | 2 | 2,5 | 3 | 5 | 10 | $\infty$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0,000 |  | 0,250 | 0,250 | 0,250 | 0,250 | 0,250 | 0,250 | 0,250 | 0,250 | 0,250 | 0,250 | 0,250 | 0,250 | 0,250 |
| 0,2 | 0,000 | 0,137 | 0,204 | 0,234 | 0,240 | 0,244 | 0,247 | 0,249 | 0,249 | 0,249 | 0,249 | 0,249 | 0,249 | 0,249 | 0,249 |
| 0,4 | 0,000 | 0,076 | 0,136 | 0,187 | 0,202 | 0,218 | 0,231 | 0,240 | 0,243 | 0,244 | 0,244 | 0,244 | 0,244 | 0,244 | 0,244 |
| 0,5 | 0,000 | 0,061 | 0,113 | 0,164 | 0,181 | 0,200 | 0,218 | 0,232 | 0,238 | 0,239 | 0,240 | 0,240 | 0,240 | 0,240 | 0,240 |
| 0,6 | 0,000 | 0,051 | 0,096 | 0,143 | 0,161 | 0,182 | 0,204 | 0.223 | 0,231 | 0,233 | 0,234 | 0,234 | 0,234 | 0,234 | 0,234 |
| 0,8 | 0,000 | 0,037 | 0,071 | 0,111 | 0,127 | 0,148 | 0,173 | 0,200 | 0,214 | 0,218 | 0,219 | 0,220 | 0,220 | 0,220 | 0,220 |
| 1 | 0,000 | 0,028 | 0,055 | 0,087 | 0,101 | 0,120 | 0,145 | 0,175 | 0,194 | 0,200 | 0,202 | 0,203 | 0,204 | 0,205 | 0,205 |
| 1,2 | 0,000 | 0,022 | 0,043 | 0,069 | 0,081 | 0,098 | 0,121 | 0,152 | 0,173 | 0,182 | 0,185 | 0,187 | 0,189 | 0,189 | 0,189 |
| 1,4 | 0,000 | 0,018 | 0,035 | 0,056 | 0,066 | 0,080 | 0,101 | 0,131 | 0,154 | 0,164 | 0,169 | 0,171 | 0,174 | 0,174 | 0,174 |
| 1,5 | 0,000 | 0,016 | 0,031 | 0,051 | 0,060 | 0,073 | 0,092 | 0,121 | 0,145 | 0,156 | 0,161 | 0,164 | 0,166 | 0,167 | 0,167 |
| 1,6 | 0,000 | 0,014 | 0,028 | 0,046 | 0,055 | 0,067 | 0,085 | 0,112 | 0,135 | 0,148 | 0,154 | 0,157 | 0,160 | 0,160 | 0,160 |
| 1,8 | 0,000 | 0,012 | 0,024 | 0,039 | 0,046 | 0,056 | 0,072 | 0,097 | 0,121 | 0,133 | 0,140 | 0,143 | 0,147 | 0,148 | 0,148 |
| 2 | 0,000 | 0,010 | 0,020 | 0,033 | 0,039 | 0,048 | 0,061 | 0,084 | 0,107 | 0,120 | 0,127 | 0,131 | 0,136 | 0,137 | 0,137 |
| 2,5 | 0,000 | 0,007 | 0,013 | 0,022 | 0,027 | 0,033 | 0,043 | 0,060 | 0,080 | 0,093 | 0,101 | 0,106 | 0,113 | 0,115 | 0,115 |
| 3 | 0,000 | 0,005 | 0,010 | 0,016 | 0,019 | 0,024 | 0,031 | 0,045 | 0,061 | 0,073 | 0,081 | 0,087 | 0,096 | 0,099 | 0,099 |
| 4 | 0,000 | 0,003 | 0,006 | 0,009 | 0,011 | 0,014 | 0,019 | 0,027 | 0,038 | 0,048 | 0,055 | 0,060 | 0,071 | 0,076 | 0,076 |
| 5 | 0,000 | 0,002 | 0,004 | 0,006 | 0,007 | 0,009 | 0,012 | 0,018 | 0,026 | 0,033 | 0,039 | 0,043 | 0,055 | 0,061 | 0,062 |
| 10 | 0,000 | 0,000 | 0,001 | 0,002 | 0,002 | 0,002 | 0,003 | 0,005 | 0,007 | 0,009 | 0,011 | 0,013 | 0,020 | 0,028 | 0,032 |
| 15 | 0,000 | 0,000 | 0,000 | 0,001 | 0,001 | 0,001 | 0,001 | 0,002 | 0,003 | 0,004 | 0,005 | 0,006 | 0,010 | 0,016 | 0,021 |
| 20 | 0,000 | 0,000 | 0,000 | 0,000 | 0,000 | 0,001 | 0,001 | 0,001 | 0,002 | 0,002 | 0,003 | 0,004 | 0,006 | 0,010 | 0,016 |
| 50 | 0,000 | 0,000 | 0,000 | 0,000 | 0,000 | 0,000 | 0,000 | 0,000 | 0,000 | 0,000 | 0,000 | 0,001 | 0,001 | 0,002 | 0,006 |

