

PROGRAM	:	BACHELOR OF ENGINEERING TECHNOLOGY
		CHEMICAL ENGINEERING
SUBJECT	:	CHEMICAL PROCESS TECHNOLOGY 1B
CODE	:	CPTCHB1
DATE	:	SUMMER EXAMINATION
		25 NOVEMBER 2019
DURATION	:	(SESSION 1) 08:30 - 11:30
<u>WEIGHT</u>	:	40 : 60
TOTAL MARKS	:	120
EXAMINER(S)	:	MR P KHANGALE
MODERATOR	:	DR L MEKUTO
NUMBER OF PAGES	:	8 PAGES
<u>REQUIREMENTS</u>	:	Use of scientific (non-programmable) calculator is permitted

(only one per candidate)

HINTS AND INSTRUCTIONS TO CANDIDATE(S):

- The purpose of this assessment is to determine not only if you can write down an answer, but also to assess whether you understand the concepts, principles and expressions involved. Set out solutions in a logical and concise manner with justification for the steps followed.
- **ATTEMPT** <u>ALL</u> **QUESTIONS**. Please answer each question to the best of your ability.
- Write your details (module name and code, ID number, student number etc.) on script(s).
- Number each question clearly; questions may be answered in any order.

QUESTION 1

1.1.	List three instruments used to measure Temperature	(3)
1.2.	Explain briefly the importance of pressure in a chemical process.	(10)

1.3. Explain briefly what is meant by gauge pressure (5)

QUESTION 2

- **2.1.** Derive the Bernoulli equation from first principles. (22)
- 2.2. Water is pumped at $0.001 \text{m}^3 \text{s}^{-1}$ to a tank through a 0.04m internal and 0.05m external diameter pipe as shown in the diagram. The frictional loss from the beginning of the system to the end, Δh_f ,

1m 6m 2bar

is 15m. The viscosity, heat capacity, thermal conductivity and the density of water is 1cP, 4200Jkg⁻¹K⁻¹, 0.6Wm⁻¹K⁻¹ and 1000kgm⁻³ respectively. What is Δh_p , the head of the pump (m)? (15)



[18]

QUESTION 3

A shell and tube heat exchanger heats 2.52 kgs⁻¹ of water from 21.1 to 54.4 °C by using hot water under pressure entering at 115.6 and leaving at 48.9 °C. The outside surface area of the tubes in the exchanger is $A_0 = 9.30 \text{ m}^2$. If this is a counter current operation, calculate:

- a) The mean temperature difference ΔTm in the exchanger. (5)
- b) The overall heat-transfer coefficient U_0 . (15)

Cp of water is 4.187 kJkg⁻¹K⁻¹

QUESTION 4

A gas of pure A at 830 kPa (8.2 atm) enters a reactor with a volumetric flow rate of 2 $dm^3 s^{-1}$ at 500 K.

- 1.1 Calculate the entering concentration of A, C_{A0} , and the entering molar flow rate, F_{A0} . Assume that the gas behave as an ideal gas with PV = nRT. (10)
- 1.2 Calculate the volume of a CSTR reactor necessary to consume 65% of A if the rate of reaction $-r_A = 0.05 \text{ mol.h}^{-1} \cdot \text{dm}^{-3}$. (10)
- 1.3 If this was a batch reactor with the same volume as CSTR, determine the time necessary to achieve the same conversion in 1.2. (5)

R=8.314 dm³.kPa.mol⁻¹.K⁻¹

QUESTION 5

A hazard and operability study (**HAZOP**) is a structured and systematic examination of a complex planned or existing process or operation in order to identify and evaluate problems that may represent risks to personnel or equipment. Explain briefly why is important to conduct HAZOP study for a chemical process

[20]

[25]

[20]

TOTAL MARKS =120

FULL MARKS =120

Quantity	Equivalent Values						
Mass	$1 \text{ kg} = 1000 \text{ g} = 0.001 \text{ metric ton} = 2.20462 \text{ lb}_{m} = 35.27392 \text{ oz}$ $1 \text{ lb}_{m} = 16 \text{ oz} = 5 \times 10^{-4} \text{ ton} = 453.593 \text{ g} = 0.453593 \text{ kg}$						
Length	$1 \text{ m} = 100 \text{ cm} = 1000 \text{ mm} = 10^6 \text{ microns} (\mu \text{m}) = 10^{10} \text{ angstroms} (Å)$ = 39.37 in. = 3.2808 ft = 1.0936 yd = 0.0006214 mile 1 ft = 12 in. = 1/3 yd = 0.3048 m = 30.48 cm						
Volume	$1 m^{3} = 1000 L = 10^{6} cm^{3} = 10^{6} mL$ = 35.3145 ft ³ = 220.83 imperial gallons = 264.17 gal = 1056.68 qt 1 ft ³ = 1728 in. ³ = 7.4805 gal = 0.028317 m ³ = 28.317 L = 28.317 cm ³						
Force	$1 \text{ N} = 1 \text{ kg} \cdot \text{m/s}^2 = 10^5 \text{ dynes} = 10^5 \text{ g} \cdot \text{cm/s}^2 = 0.22481 \text{ lb}_f$ $1 \text{ lb}_f = 32.174 \text{ lb}_m \cdot \text{ft/s}^2 = 4.4482 \text{ N} = 4.4482 \times 10^5 \text{ dynes}$						
Pressure	$1 \text{ atm} = 1.01325 \times 10^5 \text{ N/m}^2 (\text{Pa}) = 101.325 \text{ kPa} = 1.01325 \text{ bar} \\ = 1.01325 \times 10^6 \text{ dynes/cm}^2 \\ = 760 \text{ mm Hg at } 0^\circ \text{C} (\text{torr}) = 10.333 \text{ m H}_2\text{O} \text{ at } 4^\circ \text{C} \\ = 14.696 \text{ lb}_{\text{f}}/\text{in.}^2 (\text{psi}) = 33.9 \text{ ft H}_2\text{O} \text{ at } 4^\circ \text{C} \\ = 29.921 \text{ in. Hg at } 0^\circ \text{C}$						
Energy	$1 J = 1 N \cdot m = 10^{7} \text{ ergs} = 10^{7} \text{ dyne} \cdot \text{cm}$ = 2.778 × 10 ⁻⁷ kW·h = 0.23901 cal = 0.7376 ft-lb _f = 9.486 × 10 ⁻⁴ Btu						
Power	$1 \text{ W} = 1 \text{ J/s} = 0.23901 \text{ cal/s} = 0.7376 \text{ ft} \cdot \text{lb}_{\text{f}}/\text{s} = 9.486 \times 10^{-4} \text{ Btu/s}$ = $1.341 \times 10^{-3} \text{ hp}$						

	-		
Material	Coeff. per degree Celsius	Material	Coeff. per degree Celsius
Iron Nickel	0.006 0.005	Tungsten Platinum	$0.0045 \\ 0.00385$

 TABLE 5.1

 Loss coefficients for standard threaded pipe fittings^{9b}

Selected Equivalent Lengths

V		
<u>K_f</u>	Fitting	L _e /d
0.35		
0.75	Elbow, 90° standard	35
0.4	Tee, flow straight through	20
1.0	Tee, flow through bend	60
1.5	Globe valve, fully open	340
4.5	Gate Valve, fully open	25
4.J 0.17		

Fitting	K _f
Elbow, standard	
45°	0.35
90°	0.75
Tee	
Straight through	0.4
Used as elbow	1.0
Return bend, 180°	1.5
Gate valve	
Half open	4.5
Wide open	0.17
Angle valve, wide open	2.0
Globe valve, wide open	6.0

$$\Delta h_{fe} = \frac{(u_s - u_l)^2}{2g}$$

$$\Delta h_{fc} = K \frac{{u_s}^2}{2g}$$

$$K = 0.4 \left(1.25 - \left(\frac{d_s}{d_l}\right)^2 \right) \qquad \text{When} \qquad \frac{d_s^2}{d_l^2} \prec 0.715$$

$$K = 0.75 \left(1.0 - \left(\frac{d_s}{d_l}\right)^2 \right) \qquad \text{When} \qquad \frac{d_s^2}{d_l^2} \succ 0.715$$

APPENDIX 3

Dimensions, Capacities, and Weights of Standard Steel Pipe[†]

Nominal pipe size, in.	Outside diameter, in.	Schedule no.	Wall thickness, in.	Inside diameter, in.	Cross- sectional area of metal, in. ²	Inside sectional area, ft ²	Circumference, ft or surface, ft ² /ft of length		1 ft/s velocity		Pipe
							-		U.S. gal/min	Water, b	weight lb/ft
ł	0.405	40	0.068	0.269	0.072	0.00040	0.106	0.0705	0.179	89.5	0.24
		80	0.095	0.215	0.093	0.00025	0.106	0.0563	0.113	56.5	0.31
1	0.540	40	0.088	0.364	0.125	0.00072	0.141	0.095	0.323	161.5	0.42
		80	0.119	0.302	0.157	0.00050	0.141	0.079	0.224	112.0	0.54
3	0.675	40	0.091	0.493	0.167	0.00133	0.177	0.129	0.596	298.0	0.57
		+80	0.126	0.423	0.217	0.00098	0.177	0.111	0.440	220.0	0.74
1/2	0.840	40	0.109	0.622	0.250	0.00211	0.220	0.163	0.945	472.0	0.85
_		80	0.147	0.546	0.320	0.00163	0.220	0.143	0.730	365.0	1.09
34	1.050	40	0.113	0.824	0.333	0.00371	0.275	0.216	1.665	832.5	1.13
		80	0.154	0.742	0.433	0.00300	0.275	0.194	1.345	672.5	1.15
1	1.315	40	0.133	1.049	0.494	0.00600	0.344	0.275	2.690	1,345	1.68
		80	0.179	0.957	0.639	0.00499	0.344	0.250	2.240	1,120	2.17
11	1.660	40	0.140	1.380	0.668	0.01040	0.435	0.361	4.57	2,285	2.17
58		80	0.191	1.278	0.881	0.00891	0.435	0.335	3.99	1,995	3.00
11/2	1.900	40	0.145	1.610	0.800	0.01414	0.497	0.421	6.34	3,170	2.72
		80	0.200	1.500	1.069	0.01225	0.497	0.393	5.49	2,745	
2	2.375	40	0.154	2.067	1.075	0.02330	0.622	0.541	10.45	5,225	3.63
		80	0.218	1.939	1.477	0.02050	0.622	0.508	9.20	4,600	3.65
21	2.875	40	0.203	2.469	1.704	0.03322	0.753	0.647	14.92	7,460	5.02
(1 7 54		80	0.276	2.323	2.254	0.02942	0.753	0.608	13.20	6,600	5.79
3	3.500	40	0.216	3.068	2.228	0.05130	0.916	0.803	23.00		7.66
		80	0.300	2.900	3.016	0.04587	0.916	0.759	20.55	11,500	7.58
31/2	4.000	40	0.226	3.548	2.680	0.06870	1.047	0.929	30.80	10,275	10.25
		80	0.318	3.364	3.678	0.06170	1.047	0.881	27.70	15,400	9.11
4	4.500	40	0.237	4.026	3.17	0.08840	1.178	1.054	39.6	13,850	12.51
		80	0.337	3.826	4.41	0.07986	1.178	1.002	35.8	19,800	10.79
5	5.563	40	0.258	5.047	4.30	0.1390	1.456	1.321	62.3	17,900	14.98
		80	0.375	4.813	6.11	0.1263	1.456	1.260	57.7	31,150	14.62
6	6.625	40	0.280	6.065	5.58	0.2006	1.734	1.588	90.0	28,850	20.78
		80	0.432	5.761	8.40	0.1810	1.734	1.508		45,000	18.97
8	8.625	40	0.322	7.981	8.396	0.3474	2.258		81.1	40,550	28.57
	0.1990.00255	80	0.500	7.625	12.76	0.3474	2.258	2.089	155.7	77,850	28.55
10	10.75	40	0.365	10.020	11.91	0.5475			142.3	71,150	43.39
1982/97	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	80	0.594	9.562		0.4987				123,000	40.48
12	12.75	40	0.406	11.938	15.74	0.4987			223.4	111,700	64.40
10.02	0.00000000	80	0.688	11.374		0.7056				174,500 158,350	53.56 88.57

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