



**PROGRAM** : BACCALAUREUS INGENIERIAE  
*MECHANICAL ENGINEERING*

**SUBJECT** : STRENGTH OF MATERIALS 2B

**CODE** : SLR2B21

**DATE** : SUMMER EXAMINATION  
23<sup>RD</sup> NOVEMBER 2016

**DURATION** : (1-PAPER) 08:30 - 11:30

**WEIGHT** : 50 : 50

**TOTAL MARKS** : 100

**EXAMINER** : DR M. F. ERINOSHO

**MODERATOR** : DR D. M. MADYIRA

**NUMBER OF PAGES** : 6 PAGES AND 1 ANNEXURE

**INSTRUCTIONS** : QUESTION PAPERS MUST BE HANDED IN.

**REQUIREMENTS** : ANSWER BOOKLET.

**INSTRUCTIONS TO CANDIDATES:**

PLEASE ANSWER ALL THE QUESTIONS.

**QUESTION 1****20 Marks**

EMF material testing company was awarded a contract to test the strength of a stainless steel shaft for a building construction project going on in Johannesburg metropolis. The specimen to be tested is as shown in Figure 1 and the results of the test obtained on the specimen are as follows:

- Original diameter = 40 mm
- Original gauge length = 80 mm
- Final length between gauge point = 85.8 mm
- Final minimum diameter (neck) = 25.6 mm
- Proportional limit load = 120 kN
- Extension at proportional limit = 0.052 mm
- Yield point load = 135 kN
- Maximum recorded load = 210 kN

You are required to determine the following:

- (a) The modulus of elasticity for the stainless steel,
- (b) The proportional limit stress;
- (c) The ultimate tensile strength;
- (d) The percentage elongation;
- (e) The percentage reduction in area;
- (f) The modulus of toughness.
- (g) Sketch and dimension the original and the fractured specimen. (20 Marks)



Figure 1: Stainless steel shaft

**QUESTION 2****20 Marks**

(a) The slab joint as shown in Figure 2 (a) is fastened together using two bolts. Determine the required diameter of the bolts if the failure shear stress for the bolts is  $\tau_{\text{fail}} = 450 \text{ MPa}$ . Use a factor of safety for shear of F.S = 3.5. (5 Marks)

(b) The frame design is subjected to the load of 4 kN which acts on member ABD at D as shown in Figure 2 (b). If pin C is subjected to double shear and pin D is subjected to single shear, determine the required diameter of the pins at D and C if the allowable shear stress for the material is  $\tau_{\text{allow}} = 45 \text{ MPa}$ . (15 Marks)

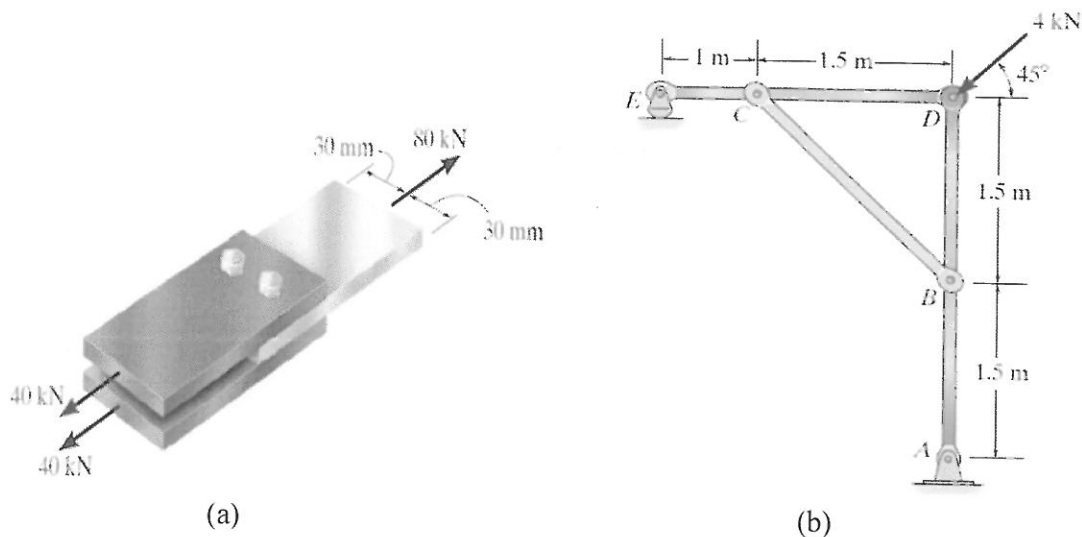


Figure 2: (a) Slab joint design; (b) Frame design

**QUESTION 3****15 Marks**

The shaft as shown in Figure 3 is made of A992 steel with the allowable shear stress of  $\tau_{\text{allow}} = 75 \text{ MPa}$ . From the shaft design, Gear B supplies 15 kW of power, while gears A, C, and D withdraw 6 kW, 4 kW, and 5 kW, respectively. If the shaft is rotating at 600 rpm, determine the following:

- The required minimum diameter  $d$  of the shaft to the nearest millimeter,
- The corresponding angle of twist of gear A relative to gear D. (15 Marks)

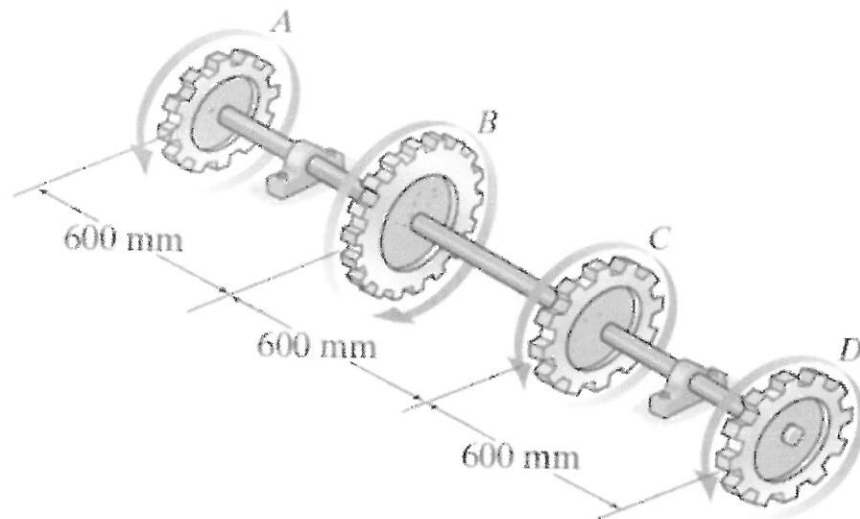


Figure 3: Shaft-gear design

**QUESTION 4****20 Marks**

The simply supported beam is built-up from three boards by nailing them together as shown in Figure 4. The wood has an allowable shear stress of  $\tau_{\text{allow}} = 1.5 \text{ MPa}$ , and an allowable bending stress of  $\sigma_{\text{allow}} = 9 \text{ MPa}$ . The nails are spaced at  $s = 75 \text{ mm}$ , and each has shear strength of  $1.5 \text{ kN}$ .

Determine:

- (i) The maximum allowable force **P** that can be applied to the beam,
- (ii) Draw the shear force and bending moment diagrams for the beam. (20 Marks)

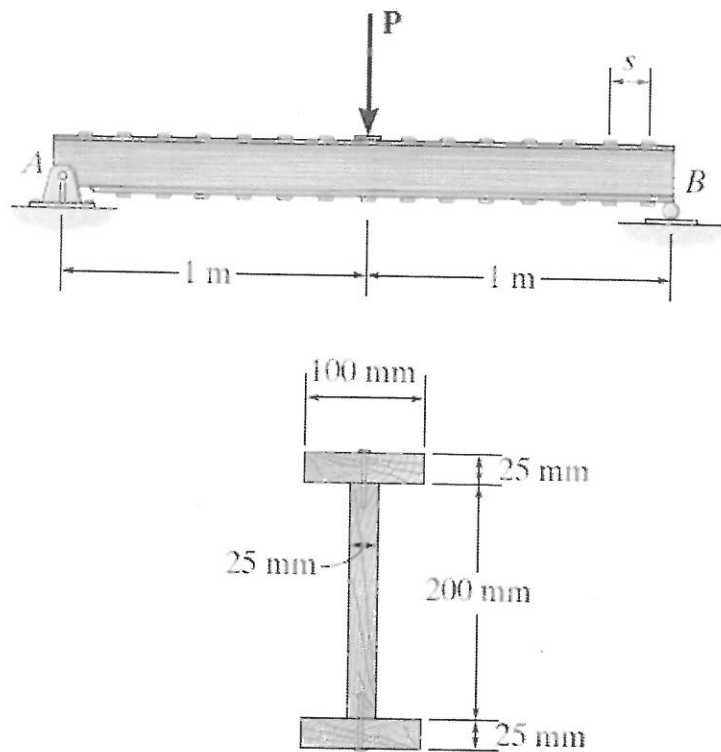


Figure 4: Simply supported beam

**QUESTION 5****25 Marks**

Figure 5 shows the equivalent state of stress at a point on the element.

Determine:

- (i) The principal stress.
- (ii) The orientation of the principal stress.
- (iii) The maximum in-plane shear stress.
- (iv) The associated average normal stress.
- (v) The corresponding orientation of the maximum in-plane shear stress
- (vi) Sketch the results on each element.

(25 Marks)

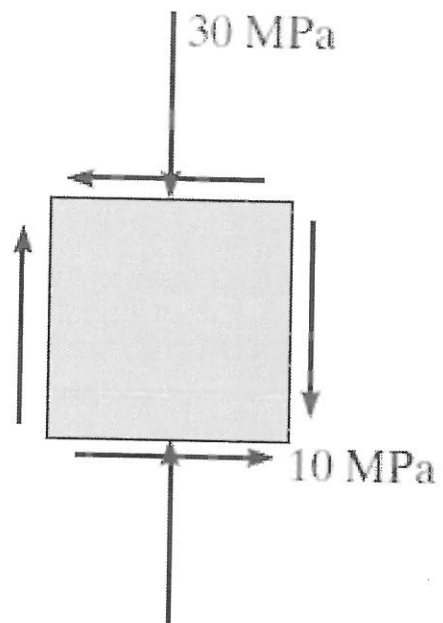


Figure 5: An element

ANNEXURE  
FORMULA SHEET

$$\sigma = \frac{P}{A} \quad ; \quad \tau_{avg} = \frac{V}{A} \quad ; \quad \sigma = E\varepsilon \quad ; \quad \tau = G\gamma \quad ; \quad \epsilon = \frac{\Delta l}{l} \times 100\% \quad ; \quad P = T\omega$$

$$\nu = \frac{-\varepsilon_{lat}}{\varepsilon_{long}} \quad ; \quad G = \frac{E}{2(1+\nu)} \quad ; \quad \tau = \frac{VQ}{It} \quad ; \quad U_r = \frac{1}{2} \frac{\sigma^2}{E} \quad ; \quad \delta = \sum \frac{PL}{AE}$$

$$q = \frac{VQ}{I} \quad ; \quad \phi = \sum \frac{TL}{JG} \quad ; \quad -w = \frac{dV}{dx} \quad ; \quad V = \frac{dM}{dx} \quad ; \quad \% \Delta A = \frac{A_o - A_f}{A_o} \times 100\%$$

$$\sigma_b = \frac{Mc}{I} \quad ; \quad I = \frac{1}{12} bD^3 \quad ; \quad \sigma_{x'} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos 2\theta + \tau_{xy} \sin 2\theta$$

$$\tau_{x'y'} = -\frac{\sigma_x - \sigma_y}{2} \sin 2\theta + \tau_{xy} \cos 2\theta \quad ; \quad \sigma_{1,2} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$\tau_{max\_in\_plane} = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} \quad ; \quad \sigma_{avg} = \frac{\sigma_x + \sigma_y}{2} \quad ; \quad \delta_t = \alpha \Delta T L$$

$$\varepsilon_{x'} = \frac{\varepsilon_x + \varepsilon_y}{2} + \frac{\varepsilon_x - \varepsilon_y}{2} \cos 2\theta + \frac{1}{2} \gamma_{xy} \sin 2\theta \quad ; \quad \varepsilon_{1,2} = \frac{\varepsilon_x + \varepsilon_y}{2} \pm \sqrt{\left(\frac{\varepsilon_x - \varepsilon_y}{2}\right)^2 + \frac{\gamma_{xy}^2}{4}}$$

$$\varepsilon_{y'} = \frac{\varepsilon_x + \varepsilon_y}{2} - \frac{\varepsilon_x - \varepsilon_y}{2} \cos 2\theta - \frac{1}{2} \gamma_{xy} \sin 2\theta \quad ; \quad \frac{\gamma_{x'y'}}{2} = -\left(\frac{\varepsilon_x - \varepsilon_y}{2}\right) \sin 2\theta + \frac{\gamma_{xy}}{2} \cos 2\theta$$

$$\gamma_{max\_in\_plane} = 2 \sqrt{\left(\frac{\varepsilon_x - \varepsilon_y}{2}\right)^2 + \frac{\gamma_{xy}^2}{4}} \quad ; \quad \varepsilon_{avg} = \frac{\varepsilon_x + \varepsilon_y}{2} \quad ; \quad \sigma = -\frac{M_y}{I_z} + \frac{M_z}{I_y}$$

$$\varepsilon_x = \frac{1}{E} (\sigma_x - \nu(\sigma_y + \sigma_z)) \quad ; \quad \varepsilon_y = \frac{1}{E} (\sigma_y - \nu(\sigma_x + \sigma_z)) \quad ; \quad \varepsilon_z = \frac{1}{E} (\sigma_z - \nu(\sigma_x + \sigma_y))$$

$$\tan 2\theta_p = \frac{2\tau_{xy}}{(\sigma_x - \sigma_y)} \quad ; \quad \tan 2\theta_s = -\left(\frac{\varepsilon_x - \varepsilon_y}{\gamma_{xy}}\right) \quad ; \quad F.S. = \frac{\sigma_y}{\sigma_{calculated}}$$

$$\sigma_1 = \frac{Pr}{t} \quad ; \quad \sigma_2 = \frac{Pr}{2t} \quad ; \quad EI \frac{d^2 y}{dx^2} = M \quad ; \quad EI \frac{d^3 y}{dx^3} = V \quad ; \quad EI \frac{d^4 y}{dx^4} = -w$$

$$J = \frac{\pi}{32} [D^4 - d^4] \quad ; \quad \tau_{allow} = \frac{Tc}{J} \quad ; \quad J = \frac{\pi}{2} C^4 \quad ; \quad K = \frac{\sigma_{max}}{\sigma_{avg}} \quad ; \quad UTS = \frac{P_{max}}{A}$$



**PROGRAM** : BACCALAUREUS INGENERIAE  
*MECHANICAL ENGINEERING*

**SUBJECT** : STRENGTH OF MATERIALS 2B

**CODE** : SLR2B21

**DATE** : SUPPLEMENTARY EXAMINATION

**DURATION** : (2-PAPER) 08:30 - 11:30

**WEIGHT** : 50 : 50

**TOTAL MARKS** : 100

**EXAMINER** : DR M. F. ERINOSHO

**MODERATOR** : DR D. M. MADYIRA

**NUMBER OF PAGES** : 5 PAGES AND 1 ANNEXURE

**INSTRUCTIONS** : QUESTION PAPERS MUST BE HANDED IN.

**REQUIREMENTS** : ANSWER BOOKLET.



**INSTRUCTIONS TO CANDIDATES:**

PLEASE ANSWER ALL THE QUESTIONS.

**QUESTION 1****18 Marks**

(a) Provide the definition for the following:

- (i) Shear force,
- (ii) Modulus of Toughness,
- (iii) Poisson's ratio,
- (iv) Strain hardening,
- (v) Necking.

*(5 Marks)*

- (b) As shown in Figure 1, member **CB** has a square cross section of 25 mm on each side. Determine the largest load **P** that can be applied to the frame without causing either the average normal stress or the average shear stress at section **a-a** to exceed  $\sigma = 150$  MPa and  $\tau = 450$  MPa, respectively.

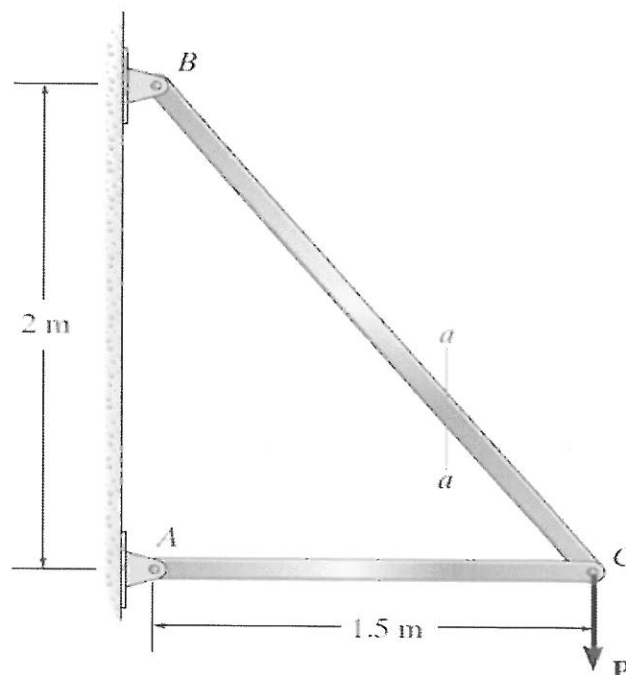
*(13 Marks)*

Figure 1: Frame

**QUESTION 2****20 Marks**

- (a) The 500 kg engine is suspended from the jib crane at the position as shown in Figure 2. Determine the state of stress at point **B** on the cross section of the boom at section **a-a**. Note that point **B** is just above the bottom flange. (20 Marks)

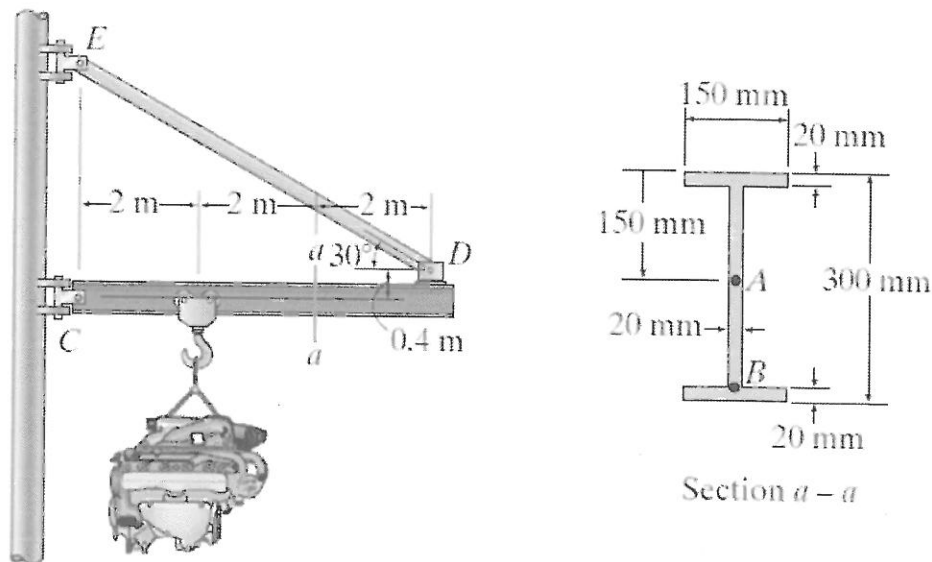


Figure 2: An engine suspension

**QUESTION 3****17 Marks**

A spring-supported pipe hanger as shown in Figure 3 consists of two springs, which are originally unstretched and have a stiffness of  $k = 60 \text{ kN/m}$ , three 304 stainless steel rods, **AB** and **CD**, which have a diameter of 5 mm, and **EF**, which has a diameter of 12 mm, and a rigid beam **GH**. If the pipe is displaced 82 mm when it is filled with fluid, determine the weight of the fluid. (17 Marks)

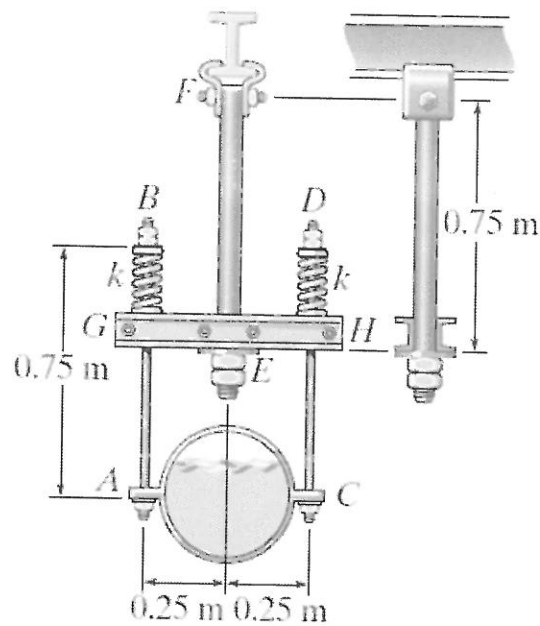


Figure 3: A spring- supported pipe hanger

**QUESTION 4****25 Marks**

The state of strain at a point as shown in Figure 4 has components of  $\epsilon_x = -300(10^{-6})$ ,  $\epsilon_y = 0$ , and  $\gamma_{xy} = -150(10^{-6})$ .

Use the strain-transformation equations to determine:

- The in-plane principal strains,
- The orientation of the principal plane,
- The maximum in-plane shear strain,
- The orientation of the maximum in-plane shear strain,
- The average normal strain,
- Show how the strains deform the element within the x-y plane.

*(25 Marks)*

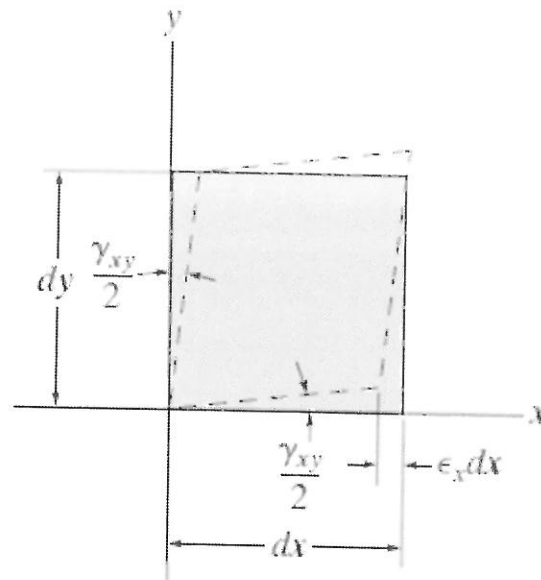


Figure 4: A component

**QUESTION 5****20 Marks**

The beam as shown in Figure 5 is supported by a pin at *A*, a roller at *B*, and a post having a diameter of 50 mm at *C*. The post and the beam are made of the same material having a modulus of elasticity  $E = 200 \text{ GPa}$ , and the beam has a constant moment of inertia  $I = 255(10^6) \text{ mm}^4$ . Determine the support reactions at *A*, *B*, and *C*. (20 Marks)

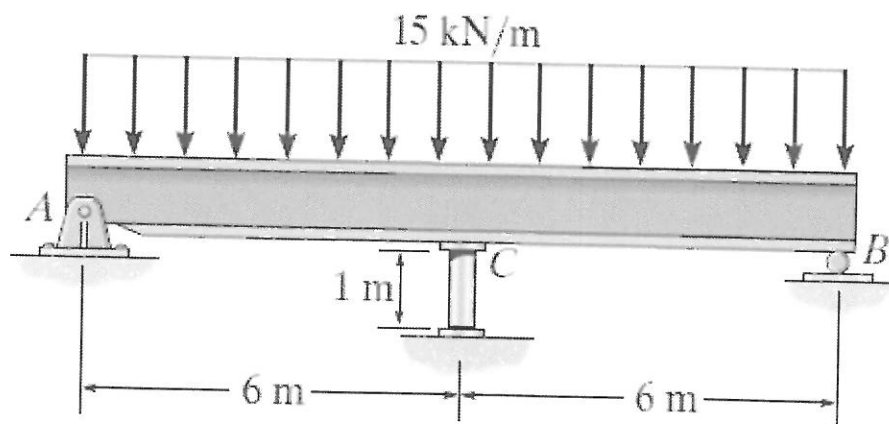


Figure 5: A supported beam

**ANNEXURE  
FORMULA SHEET**

$$\sigma = \frac{P}{A} \quad ; \quad \tau_{avg} = \frac{V}{A} \quad ; \quad \sigma = E\varepsilon \quad ; \quad \tau = G\gamma \quad ; \quad \varepsilon = \frac{\Delta l}{l} \times 100\% \quad ; \quad P = T\omega$$

$$\nu = \frac{-\varepsilon_{lat}}{\varepsilon_{long}} \quad ; \quad G = \frac{E}{2(1+\nu)} \quad ; \quad \tau = \frac{VQ}{It} \quad ; \quad U_r = \frac{1}{2} \frac{\sigma^2}{E} \quad ; \quad \delta = \sum \frac{PL}{AE}$$

$$q = \frac{VQ}{I} \quad ; \quad \phi = \sum \frac{TL}{JG} \quad ; \quad -w = \frac{dV}{dx} \quad ; \quad V = \frac{dM}{dx} \quad ; \quad \% \Delta A = \frac{A_o - A_f}{A_o} \times 100\%$$

$$\sigma_b = \frac{Mc}{I} \quad ; \quad I = \frac{1}{12} bD^3 \quad ; \quad \sigma_{x'} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos 2\theta + \tau_{xy} \sin 2\theta$$

$$\tau_{x'y'} = -\frac{\sigma_x - \sigma_y}{2} \sin 2\theta + \tau_{xy} \cos 2\theta \quad ; \quad \sigma_{1,2} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$\tau_{\max\_in\_plane} = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} \quad ; \quad \sigma_{avg} = \frac{\sigma_x + \sigma_y}{2} \quad ; \quad \delta_t = \alpha \Delta T L$$

$$\varepsilon_{x'} = \frac{\varepsilon_x + \varepsilon_y}{2} + \frac{\varepsilon_x - \varepsilon_y}{2} \cos 2\theta + \frac{1}{2} \gamma_{xy} \sin 2\theta \quad ; \quad \varepsilon_{1,2} = \frac{\varepsilon_x + \varepsilon_y}{2} \pm \sqrt{\left(\frac{\varepsilon_x - \varepsilon_y}{2}\right)^2 + \frac{\gamma_{xy}^2}{4}}$$

$$\varepsilon_{y'} = \frac{\varepsilon_x + \varepsilon_y}{2} - \frac{\varepsilon_x - \varepsilon_y}{2} \cos 2\theta - \frac{1}{2} \gamma_{xy} \sin 2\theta \quad ; \quad \frac{\gamma_{x'y'}}{2} = -\left(\frac{\varepsilon_x - \varepsilon_y}{2}\right) \sin 2\theta + \frac{\gamma_{xy}}{2} \cos 2\theta$$

$$\gamma_{\max\_in\_plane} = 2 \sqrt{\left(\frac{\varepsilon_x - \varepsilon_y}{2}\right)^2 + \frac{\gamma_{xy}^2}{4}} \quad ; \quad \varepsilon_{avg} = \frac{\varepsilon_x + \varepsilon_y}{2} \quad ; \quad \sigma = -\frac{M_z y}{I_z} + \frac{M_y z}{I_y}$$

$$\varepsilon_x = \frac{1}{E} (\sigma_x - \nu(\sigma_y + \sigma_z)) \quad ; \quad \varepsilon_y = \frac{1}{E} (\sigma_y - \nu(\sigma_x + \sigma_z)) \quad ; \quad \varepsilon_z = \frac{1}{E} (\sigma_z - \nu(\sigma_x + \sigma_y))$$

$$\tan 2\theta_p = \frac{2\tau_{xy}}{(\sigma_x - \sigma_y)} \quad ; \quad \tan 2\theta_s = -\left(\frac{\varepsilon_x - \varepsilon_y}{\gamma_{xy}}\right) \quad ; \quad F.S. = \frac{\sigma_y}{\sigma_{calculated}}$$

$$\sigma_1 = \frac{Pr}{t} \quad ; \quad \sigma_2 = \frac{Pr}{2t} \quad ; \quad EI \frac{d^2 y}{dx^2} = M \quad ; \quad EI \frac{d^3 y}{dx^3} = V \quad ; \quad EI \frac{d^4 y}{dx^4} = -w$$

$$J = \frac{\pi}{32} [D^4 - d^4] \quad ; \quad \tau_{allow} = \frac{Tc}{J} \quad ; \quad J = \frac{\pi}{2} C^4 \quad ; \quad K = \frac{\sigma_{max}}{\sigma_{avg}} \quad ; \quad UTS = \frac{P_{max}}{A}$$