



**PROGRAM** : BACCALAUREUS INGENERIAE  
CIVIL ENGINEERING

**SUBJECT** : GEOTECHNICAL ENGINEERING 3A

**CODE** : GTG3B21

**DATE** : EXAMINATION  
NOV 2014

**DURATION** : 08:30 - 11:30

**WEIGHT** : 50:50

**TOTAL MARKS** : 100

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**EXAMINER** : DR FN OKONTA

**MODERATOR** : DR HA QUAINOO

**NUMBER OF PAGES** : 3 PAGES AND 2 ANNEXURES

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**INSTRUCTIONS** : QUESTION PAPERS MUST BE HANDED IN.

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**INSTRUCTIONS TO CANDIDATES:**

PLEASE ANSWER ALL THE QUESTIONS.

PLEASE NUMBER ALL QUESTIONS EXACTLY AS QUESTION PAPER.

**QUESTION 1 (20 MARKS)**

1.1) a) Compute the induced vertical stress by a rectangular uniformly loaded area of  $q = 100\text{kPa}$  and dimensions  $L=4.5$  and  $B=3$ , using the approximate method. b) what would the slope  $1H:xV$  be for the average induced stress at  $z_f$  computed by the method in 1.1 be to equate to a value at the same depth computed using analytical solution (ie would it be flatter or steeper than  $1H:2V$ , and why). (13)

1.2). Of the methods available to compute vertically induced stresses by a uniformly loaded platform, which method would you use and why, highlight both advantages and disadvantages of the chosen method. (7)

**QUESTION 2 (20 MARKS)**

2.1) Explain why the stress-strain curve from the oedometer test is normally represented by the plot of void ratio instead of strain on the vertical axis, (7)

2.2) A consolidation test is being performed on a 75.0mm diameter saturated soil specimen that had an initial height 20mm and an initial  $w=38.8\%$ . If  $G_s = 2.69$  a) compute the initial void ratio, b) if 10% reduction in the sample size occurs after minutes of starting the test, compute the final void ratio, c) the resulting strain (13)

**QUESTION 3 (20 MARKS)**

3.1). A consolidation test has been performed on a sample obtained from a saturated clay at a point 6.5m below the ground surface. The groundwater table is at the ground surface and the unit weight of the clay is  $18.5\text{kN/m}^3$ . The measured preconsolidation stress was  $260\text{kPa}$ . a) determine is the soil is normally consolidated or not, b) compute the overconsolidation margin and the overconsolidation ratio, c) compute the preconsolidation stress at a depth 12m in the same soil. (10)

3.2) Explain the terms overconsolidation margin and the overconsolidation ratio, and discuss associated errors in using the overconsolidation ratio over such depths as stated in 3.1) (10)

**QUESTION 4 (20 MARKS)**

4.1) Discuss the shortcomings of the Log-Time method and why you would recommend the Square Root of time method in determining the time-settlement curve. (5)

4.2) A 12.0m thick clay stratum with a double drainage is to be subjected to an induced stress from a 4.5m high proposed fill with  $e = 1.13$  and  $G_s = 2.68$ . If  $c_v = 3.5 \times 10^{-3} \text{ m}^2/\text{day}$  compute the hydrostatic, excess and total pore water pressure, at a point 2.7m into the clay layer 10 years after load was applied (15)

### QUESTION 5 (20 MARKS)

5.1) Slope stability analysis reveal that under geostatic stresses the slope is safe, describe ways that may destabilize the slope. (10)

5.2) Determine the effective normal stress that produces an  $\text{FoS} = 2.5$  at a point in a strata that is subject to a shear stress of 10kPa, and shear strength is defined by equation 1. (10)

$$\tau = 10 + \sigma' \tan 28 \quad \dots\dots\dots (1.1)$$

### YOU MAY USE ANY OF THE FOLLOWING EQUATIONS AND TABLES

$$e = (1 - \varepsilon_z)(1 + e_0) - 1 \quad U = \left[ 1 - 10^{-\left(\frac{0.085 + T_v}{0.933}\right)} \right] \times 100\% \quad U = \sqrt{\frac{4T_v}{\pi}} \times 100\%$$

$$\sigma'_{z0} = \sum \gamma H - u \quad \delta_{c,ult} = \sum \left( \frac{Cc}{1 + e_0} \right) H \log \left( \frac{\sigma'_{zf}}{\sigma'_{z0}} \right) \quad \rho_d = \frac{M_s}{V}$$

$$S = \frac{wG_s}{e} \times 100\% \quad G_s = \frac{M_s}{V_s \rho_w} \quad e = \frac{G_s \gamma_w}{\gamma_d} - 1$$

$$\gamma_d = \quad \sigma'_m = \sigma'_c - \sigma'_{z0} \quad OCR = \frac{\sigma'_c}{\sigma'_{z0}}$$

$$\gamma_{sat} = \frac{G_s + e}{1 + e} \gamma_w \quad \delta_{c,ult} = \sum \left( \frac{Cr}{1 + e_0} \right) H \log \left( \frac{\sigma'_{zf}}{\sigma'_c} \right) + \left( \frac{Cc}{1 + e_0} \right) H \log \left( \frac{\sigma'_c}{\sigma'_{z0}} \right)$$

$$T_v = \frac{c_v t}{H_{dr}^2} \quad \sigma'_h = K \sigma'_v \quad I = \frac{LB}{(L + zf)(B + zf)}$$

$$\frac{u_e}{\Delta \sigma_z} = \sum_{N=0}^{\infty} \left( \frac{4}{(2N + 1)\pi} \sin \left[ \frac{(2N + 1)\pi}{2} \left( \frac{z_{dr}}{H_{dr}} \right) \right] e^{-\left[ \frac{(2N + 1)^2 \pi^2}{4} T_v \right]} \right)$$

$$\delta_{c,ult} = \sum \left( \frac{Cc}{1 + e_0} \right) H \log \left( \frac{\sigma'_{z0} + \gamma_{fill} H_{fill}}{\sigma'_{z0}} \right)$$

$$\delta_{c,ult} = \sum \left( \frac{Cr}{1 + e_0} \right) H \log \left( \frac{\sigma'_{zf}}{\sigma'_c} \right) + \left( \frac{Cc}{1 + e_0} \right) H \log \left( \frac{\sigma'_c}{\sigma'_{z0}} \right)$$

