

**PROGRAM** 

: BACCALAUREUS INGENERIAE

CIVIL ENGINEERING

**SUBJECT** 

: Hydraulic Engineering 3B

CODE

: HMG3B21

DATE

: SSA EXAMINATION

2 DECEMBER 2014

<u>DURATION</u> : 3 HRS (SESSION 2) 11:30 – 14:30

WEIGHT

: 50:50

TOTAL MARKS : 100

ASSESSOR

: DR MO DINKA

MODERATOR : DR MS MAGOMBEYI File Number: HMG3B 2014

**NUMBER OF PAGES** : 3 PAGES AND 2 ANNEXURES

**INSTRUCTIONS** 

: QUESTION PAPERS MUST BE HANDED IN.

**REQUIREMENTS** : 2 SHEETS OF PAPER.

#### **INSTRUCTIONS TO STUDENTS:**

PLEASE ANSWER ALL THE QUESTIONS.

PROVIDE SHORT AND PRECISE ANSWERS FOR THE THEORETICAL PART

SHOW ALL THE STEPS FOR CALCULATIONS CLEARLY

### PART I: FLOOD HYDROLOGY [50]

### QUESTION 1: THEORY [20 Marks]

- a) As an engineer, why would you need Depth-Duration-Frequency curves? (3)
  b) Distinguish between stochastic and deterministic methods for the determination of flood peaks. Give an example for each. (6)
  c) Discuss the formation of convective precipitation in South Africa. Write the conditions (stepwise) to be satisfied for the formation of convective precipitation. (4)
  d) Why is Area Reduction Factor (ARF) applied to adjust rainfall in an area? (3)
  e) Define the following terms briefly: (4)
  - (i) Coalescence (ii) Dew point temperature

### **QUESTION 2** [15 Marks]

Given a stream with the following records of monthly mean runoff:

| Time (month)                | J  | F   | M  | A | M | J | J | A | S  | 0 | N  | D  | J  | F  | M  |
|-----------------------------|----|-----|----|---|---|---|---|---|----|---|----|----|----|----|----|
| Runoff (* $10^6$ m $^3$ /s) | 94 | 122 | 45 | 5 | 5 | 2 | 0 | 2 | 16 | 7 | 72 | 92 | 21 | 55 | 53 |

Use the Sequent Peak and Ripple Methods to find the storage required to maintain a constant yield of 23 Mm<sup>3</sup>/s per month from that stream.

#### **QUESTION 3** [15 Marks]

The air temperature measured at sea level is 18 °C, the specific humidity is  $0.005 \text{ kg H}_2\text{O/kg}$  air and air pressure is measured as 130 KPa. The air is now lifted orographically through a height of 1650 m above sea level. Take Ra = 287 J/Kg/K

- (a) Saturated and actual vapour pressures (mb) (4)
- (b) Dew point temperature (°C) (3)
- (c) Relative humidity (%)
- (d) Air density  $(kg/m^3)$  (3)
- (e) Is it likely that it will rain? (3)

### PART II: OPEN CHANNEL [50]

#### **QUESTION 4. THEORY [20 Marks]**

### Answer the following questions in short and precise.

- (a) Derive the relation between Chezy C and Darcey-Weisbatch f.
- (b) Define the occurrence of hydraulic jump and explain its advantage and disadvantages.
- (c) Derive equation of energy loss due to hydraulic jump from basic principle. (8)

#### QUESTION 5 [30 Marks]

Water flows at a rate of 120 m<sup>3</sup>/s in a rectangular channel with bottom width of 8m and side slope of 1:2 (V:H). The water flows out freely at the end of the channel. The long section of the channel is shown in the figure Q5 bellow. Manning's n is 0.014.

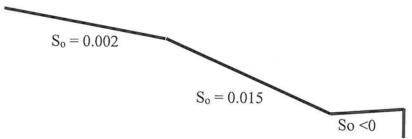


Figure Q5

- a) Calculate the normal flow depth and velocity (4)
- b) Calculate critical flow: depth, velocity and slope (4)
- c) Determine the flow depth upstream and downstream of the hydraulic jump (4)
- d) Identify all control points in the channel and determine the flow depths at all the control points (6)
- e) Draw and identify the flow profiles for a flow depth of 0.8 m (4)
- f) Calculate the following if hydraulic jump occurs. (8)
  - (i) Downstream flow depth
  - (ii) Energy loss in the channel
  - (iii) Velocity downstream of the hydraulic jump
  - (iv) Height of the jump
  - (v) Length of the jump

## FORMULA SHEET

# Flood Hydrology

| $p = 1 - \left(1 - \frac{1}{T}\right)^N$  | $G_2 = \left(\frac{I_1 + I_2}{2}\right) + G_1 - C_2$              | $Q_2 = C_2 I_1 + C_1 I_2 + C_3 Q_1$   |  |  |  |  |  |
|---|---|---|--|--|--|--|--|
| i = regional factor = factor  | MAP factor × frequenc   | $C_1 = \frac{K \times X + 0.5 \times X}{K - K \times X + 0.5}$  | $\frac{\Delta t}{\Delta t} = Q = \chi A_e^{\gamma}$  |  |  |  |  |
| regional factor (coas   | stal) = $\frac{122.8}{(1 + 4.779 \times t)^{0.73}}$               | $C_2 = \frac{-K \times X + 0.5 \times 10^{-10}}{K - K \times X + 0.5}$                                  | $\frac{\Delta t}{\Delta t} = \frac{a \cdot N + b}{c \cdot m + d}$  |  |  |  |  |
| regional factor (inla   | $1d) = \frac{217.8}{(1 + 4.164 \times t)^{0.883}}$                | $C_{3} = \frac{K - K \times X - 0.5}{K - K \times X + 0.5}$   | $\frac{\times \Delta t}{\times \Delta t}  C_1 + C_2 + C_3 = 1$   |  |  |  |  |
| MAP factor = $\frac{18.79}{}$   | + 0.17 × MAP<br>100   | $\frac{\Delta t}{2(1-X)} \le K \le \frac{\Delta t}{2X}$   | $S = \frac{a}{b+1} \times h^{b-1}$   |  |  |  |  |
| ARF = (90 000 - 12  | $800 \ln A + 9 830 \ln t)^{0}$                                    | $S_{\text{support}} = \frac{a}{b+1} \times \left[ (h_{\text{F}})^{-1} \right]$                          | $S_{\text{temporary}} = \frac{a}{b+1} \times \left[ \left( h_{\text{FSL}} + h_{\text{evenflow}} \right)^{b+1} - h_{\text{FSL}}^{-b+1} \right]$ |  |  |  |  |
| $Q = C \times i \times A$   | $t_c = \left(\frac{0.87 \times L^2}{1.000 \times S}\right)^{0.3}$ | $Q_p = K_n \times \frac{A}{T_L}$  | $Q = 10^5 \times \left(\frac{A}{10^5}\right)^{1-0.1K}$   |  |  |  |  |
| $T_{L} = C_{r} \left( \frac{L \cdot L_{c}}{\sqrt{S}} \right)^{0.36}$  | $\frac{V_t}{V_{to}} = 0.376 \ln\left(\frac{\tau}{3.5}\right)$     | $Q = K \times h_{\text{everlow}}^{\frac{3}{2}}$   | $K = \frac{2}{1+x}$  |  |  |  |  |
| $P_{t,T} = 1.13(0.41 + 0.64 \ln T)(-0.11 + 0.27 \ln t)(0.79M^{0.69}R^{0.2}) A = a^{\frac{1}{b+1}} \times (b+1)^{\frac{b}{b+1}} \times S^{\frac{b}{b+1}}$  |   |   |  |  |  |  |  |
| $C_T = \frac{C_2}{100} + \left(\frac{Y_T}{2.33}\right) \left(\frac{C_{100}}{100} - \frac{C_2}{100}\right) \qquad p = 1 T \qquad G = \frac{\text{outflow}}{2} + \frac{\text{temporary storage}}{\Delta t}$ |   |   |  |  |  |  |  |
| $e = 611 \exp \left[ \frac{17.27 * T_d}{237.3 + T_d} \right]  e_s = 611 \exp \left[ \frac{17.27 * T}{237.3 + T} \right]  q_v = 0.622 \frac{e}{P}  RH = \frac{e}{e_s}  \rho_a = \frac{P}{R_a T}$           |   |   |  |  |  |  |  |
| $Runoff \ Depth = \frac{V_{DRH}}{A} $ $K > \Delta t > 2KX$  |   |   |  |  |  |  |  |
| $\frac{\Delta t}{2(1-X)} \le K \le \frac{\Delta t}{2X}$   | $K = \frac{\Delta L}{c} \qquad K_{i} = K_{i} = K_{i}$             | $R_{t} - Q_{t} + K_{t-1} \text{ if } R_{t} - Q_{t} + K_{t-1} $<br>$K_{t-1} R_{t} - Q_{t} + K_{t-1} < 0$ | $-K_{t-1}\geq 0$   |  |  |  |  |

# FORMULA SHEET

# **Open Channel Flow**

| $v = \frac{K_u}{n} R^{2/3} S^{1/2}$                                  | $h_f = \frac{f.L}{D} \frac{V^2}{2g}$                               | $R_e = \frac{\rho vL}{\mu}$   | $h_f = S_o L$                                       |  |
|--|--|---|---|--|
| $\tau_o = \rho g R S_o$  | $F_r = \frac{v}{\sqrt{gh}}$  | $S_o = S_w = S_f$   | $Q = A_1 v_1 = A_2 v_2$                             |  |
| $Q = \sum_{i=1}^{n} V_i A_i$   | $V_i = \frac{K_u}{n_i} \left(\frac{A_i}{P_i}\right)^{2/3} S^{1/4}$ | $K = \frac{K_u}{n} A R^{2/3}$   | $n = 0.13 \frac{d^{1/6}}{g^{0.5}}$                  |  |
| $H_j = (y_2 - y_1)$  | $H = Z + y + \frac{\alpha v^2}{2g}$                                | $E_1 = E_2 + \Delta z$  | $\Delta E = \frac{(y_2 - y_1)^3}{4y_1 y_2}$         |  |
| $y_c = \left(\frac{q^2}{g}\right)^{1/3}$                             | $E_s = y + \frac{\alpha v^2}{2g}$                                  | $v = C\sqrt{R S}$   | $c = \sqrt{gy_1}$                                   |  |
|  |  | $= \sqrt{\frac{gy_2}{2y_1} [(y_2 + y_1)] + v_1}$                      | $h = \left(\frac{fL}{D}\right) \frac{V^2}{2g}$      |  |
| $\frac{y_2}{y_1} = \frac{1}{2} \left[ \sqrt{1 + 8F_1^2} - 1 \right]$ |  | $=5$ to $7*(y_2-y_1)$   | $v_w = \sqrt{\frac{gy_2}{2y_1}[(y_2 + y_1)]} + v_1$ |  |
| $H_j = 5$ to $7*(y_2 - y_1)$   |  | $= \frac{Q}{A} = \frac{V_1 A_1 + V_2 A_2 + V_3 A_3}{A_1 + A_2 + A_3}$ |   |  |