



<u>PROGRAM</u>	: NATIONAL DIPLOMA) <i>ENGINEERING: MECHANICAL</i>
<u>SUBJECT</u>	: STEAM PLANT
<u>CODE</u>	: SMP 301
<u>DATE</u>	: SUMMER EXAMINATION 2015 16 NOVEMBER 2015
<u>DURATION</u>	: (SESSION 1) 08:30 - 11:30
<u>WEIGHT</u>	:
<u>TOTAL MARKS</u>	: 114 = 100%
MAXIMUM MARKS	:
<u>ASSESSOR</u>	: ASSESSOR: Mr. E. BAKAYA-KYAHURWA
<u>MODERATOR</u>	: MODERATOR: Mr. Kobus Van Tonder
<u>NUMBER OF PAGES</u>	: PAGES: 3 excluding the cover page.
<u>INSTRUCTIONS</u>	: ONLY ONE POCKET CALCULATOR PER CANDIDATE MAY BE USED. 1. This paper contains <b>5</b> questions 2. PLEASE ANSWER ALL QUESTIONS 3. Make sure that you understand what the question requires before attempting it. 4. Any additional examination material is to be placed in the answer book and must indicate clearly the question number, and Student number. 5. Draw proper sketches where required with all relevant information Answers without calculations will not be considered. Answers without units will not be considered. All answers to be to the 4th decimal point. Number all answer according to the numbering in question paper.
<u>REQUIREMENTS</u>	: h-s Chart for steam, Thermodynamic Property Tables

**QUESTION 1**

- 1.1 The basic Rankine thermodynamic cycle does not convert heat into work at the optimum level and its performance can be improved by certain enhancements, either to the cycle itself or to the output from the cycle, which ultimately result in better fuel economy. For each of the following explain in detail the fundamental principles which enhance the performance of the cycle.  
Where appropriate cycle diagrams or flow diagrams should be included to illustrate the enhancement.
- 1.1.1 Feedwater heating in a steam cycle as used in a large scale electric power generating plant. (2)
- 1.1.2 Reheating of the steam after expansion in HP turbine (2)
- 1.1.3 Lowering the condenser pressure. (2)
- 1.2 An ideal Rankine Cycle operates at a pressure of 6 MPa with superheating to 400°C. Steam is extracted from the turbine at 0.6 MPa for feed water heating in a direct contact heat exchanger which operates at this pressure. Complete mixing of the steam and water occurs. A condensate extraction pump is required to pump from the condenser pressure of 0.004MPa to 0.6 MPa. Isentropic conditions prevail in the pumps and turbine.
- 1.2.1 Sketch the process on the Ts diagram labelling all the key points by the number corresponding to the plant diagram (10)
- 1.2.2 Determine the fractional mass flow of steam required for feed water heating (2)
- 1.2.3 Calculate the cycle efficiency with feed water heater in operation (5)

**[23]**

$$v_f @ 4 \text{ kPa} = 0.0010041 \text{ m}^3/\text{kg}$$

**QUESTION 2**

- 2.1 The walls of a furnace consist of parallel layers in contact of cement, brick and wood of thickness 20 mm, 300 mm and 10 mm respectively. Find the quantity of heat that passes through each  $\text{m}^2$  of wall per minute, if the temperature of air in contact with the wall is 5°C and 300°C inside. The values of  $k$  for cement, brick and wood are 0.294, 0.252 and 0.168 W/mK respectively. [10]
- 2.2 A steam pipe 20 m long, 100 mm internal diameter and 40 mm thick is covered by a layer of lagging of 25 mm thick. The coefficient of thermal conductivities for the pipe material and lagging are 0.07 W/m K and 0.1 W/mK respectively. If the steam is conveyed at a pressure of 1.7 MPa with 30°C superheat and the outside temperature of the lagging is 24°C, determine:  
2.2.1 the heat lost per hour (9)  
2.2.2 the interface temperature. (1)  
Neglect the pressure drop across the steam pipe.

**[20]**

**QUESTION 3**

- 3.1 Two airstreams A and B are mixed steadily and adiabatically in a ratio of 2 parts of A to 3 parts of B. Stream A enters the mixing chamber at  $40^{\circ}\text{C}$  with a relative humidity of 35%, while stream B enters with a dry bulb and wet bulb temperature of  $15^{\circ}\text{C}$  and  $12^{\circ}\text{C}$ . Assuming that the mixing process occurs at a pressure of 101.325 kPa, determine for the mixture the:
- 3.1.1 dry-bulb temperature, (3)
  - 3.1.2 moisture content, (3)
  - 3.1.3 percentage saturation, (3)
  - 3.1.4 specific enthalpy, (3)
  - 3.1.5 dew point temperature. (3)
  - 3.1.6 partial pressure of water vapour in the mixture (3)
- 3.2 A cooling tower must cool 340 kg of water per minute. The water is supplied at  $42^{\circ}\text{C}$  and it sprayed down into the column of air which enters the bottom of the tower at a rate of 540  $\text{m}^3/\text{min}$  with a temperature of  $18^{\circ}\text{C}$  and relative humidity of 60%. The moist air leaves the top of the tower saturated at  $27^{\circ}\text{C}$ . The whole process occurs at a constant pressure of 1.013 bar. Determine the temperature of the cooled water in the pool and the rate at which make up water must be supplied to replace that evaporated. (16)  
**[34]**

**QUESTION 4**

One stage of a steam turbine receives steam at a mass flow rate of 30 kg/s. The fixed blade outlet angle is  $20^{\circ}$ . The moving blade is symmetrical such that the moving blade outlet angle is equal to the moving blade inlet angle.

The initial absolute velocity of steam leaving the fixed blades is 450 m/s. the blade velocity is 250 m/s. Due to friction in the moving blades the outlet relative steam velocity from the moving blades is equal to 0.95 of the inlet relative steam velocity to these blades.

Draw to scale a velocity diagram for this turbine stage, find all the velocities and angles not stated and determine the following. (6)

- 4.1 Final absolute steam velocity leaving the moving blades and its direction (4)
- 4.2 Power developed in this stage due to change in momentum of the steam (2)
- 4.3 Blade diagram efficiency related to the energy and flow of the initial steam jet (2)

**[14]**

**QUESTION 5**

A convergent divergent nozzle is required to pass 1.8 kg of steam per sec. At inlet the steam pressure and actual temperature are 0.7 MPa and 186.2°C respectively and the speed is 75 m/sec. Expansion is stable throughout to the exit pressure of 110 kPa. There is no loss by friction in the converging section of the nozzle but loss by friction between throat and outlet is equivalent to 70 kJ/kg of steam. Calculate, assuming throat pressure of 4 bar:

- 5.1 the required area of throat in mm<sup>2</sup>. (11)  
5.2 the required area of outlet in mm<sup>2</sup>. (5)  
5.3 the overall efficiency of the nozzle, based on the heat drop between the actual inlet pressure and temperature and the outlet pressure. (7)

[23]

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**TOTAL = 114**

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# Properties of Water and Saturated Steam

$P$	$t_s$	$v_g$	$h_f$	$h_{fg}$	$h_g$	$s_f$	$s_g$
kPa	°C	m³/kg	kJ/kg	kJ/kg	kJ/kg	kJ/kg.K	kJ/kg.K
1,0	7,0	129,20	29	2 485	2 514	0,106	8,977
1,5	13,0	87,98	55	2 471	2 526	0,196	8,829
2,0	17,5	67,01	74	2 460	2 534	0,261	8,725
2,5	21,1	54,26	89	2 452	2 541	0,312	8,644
3,0	24,1	45,67	101	2 445	2 546	0,354	8,579
3,5	26,7	39,48	112	2 439	2 551	0,391	8,523
4,0	29,0	34,80	121	2 433	2 554	0,423	8,476
4,5	31,0	31,14	130	2 428	2 558	0,451	8,434
5,0	32,9	28,19	138	2 424	2 562	0,476	8,396
5,5	34,6	25,77	145	2 420	2 565	0,500	8,362
6,0	36,2	23,74	152	2 416	2 568	0,521	8,331
6,5	37,7	22,02	158	2 413	2 571	0,541	8,303
7,0	39,0	20,53	163	2 410	2 573	0,559	8,277
7,5	40,3	19,24	169	2 406	2 575	0,576	8,252
8,0	41,6	18,10	174	2 403	2 577	0,593	8,230
8,5	42,7	17,10	179	2 401	2 580	0,608	8,208
9,0	43,8	16,20	183	2 398	2 581	0,622	8,188
9,5	44,8	15,40	188	2 395	2 583	0,636	8,169
10	45,8	14,67	192	2 393	2 585	0,649	8,151
11	47,7	13,42	200	2 388	2 588	0,674	8,118
12	49,5	12,36	207	2 384	2 591	0,696	8,087
13	51,1	11,47	214	2 380	2 594	0,717	8,059
14	52,6	10,69	220	2 377	2 597	0,737	8,033
15	54,0	10,02	226	2 373	2 599	0,755	8,009
16	55,3	9,433	232	2 370	2 602	0,772	7,987
17	56,6	8,911	237	2 367	2 604	0,788	7,966
18	57,8	8,445	242	2 364	2 606	0,804	7,946
19	59,0	8,027	247	2 361	2 608	0,818	7,927
20	60,1	7,650	252	2 358	2 610	0,832	7,909
21	61,1	7,307	256	2 356	2 612	0,845	7,893
22	62,2	6,995	260	2 353	2 613	0,858	7,876
23	63,1	6,709	264	2 351	2 615	0,870	7,861
24	64,1	6,447	268	2 349	2 617	0,882	7,846
25	65,0	6,204	272	2 346	2 618	0,893	7,832
26	65,9	5,980	276	2 344	2 620	0,904	7,819
27	66,7	5,772	279	2 342	2 621	0,915	7,806
28	67,6	5,579	283	2 340	2 623	0,925	7,793
29	68,3	5,398	286	2 338	2 624	0,935	7,781
30	69,1	5,229	289	2 336	2 625	0,944	7,770

$\rho$	$t_s$	$v_g$	$h_g$	$s_i$	$s_v$	$p$	$t_s$	$v_g$	$h_g$	$s_i$	$s_v$
kPa	°C	m³/kg	kJ/kg	kJ/kg	kJ/kg	kPa	°C	m³/kg	kJ/kg	kJ/kg	kJ/kg
32	70,6	4,922	296	2,332	2,628	0,962	7,747	141,8	0,485 1	597	2,139
34	72,0	4,650	302	2,329	2,631	0,980	7,727	142,7	0,473 4	601	2,136
36	73,4	4,408	307	2,326	2,633	0,996	7,707	143,6	0,462 2	605	2,133
38	74,7	4,190	313	2,322	2,635	1,011	7,688	144,5	0,451 6	609	2,130
40	75,9	3,993	318	2,319	2,637	1,026	7,671	145,4	0,441 5	612	2,128
45	78,7	3,576	330	2,312	2,642	1,060	7,631	146,3	0,431 8	616	2,125
50	81,4	3,240	341	2,305	2,646	1,091	7,595	147,1	0,422 6	620	2,122
55	83,7	2,964	351	2,299	2,650	1,119	7,562	147,9	0,413 8	624	2,120
60	86,0	2,732	360	2,294	2,654	1,145	7,533	148,7	0,405 3	627	2,117
65	88,0	2,535	369	2,288	2,657	1,170	7,506	149,5	0,397 2	630	2,115
70	90,0	2,365	377	2,283	2,660	1,192	7,480	150,3	0,389 4	634	2,112
75	91,8	2,217	385	2,279	2,664	1,213	7,457	151,1	0,381 9	637	2,110
80	93,5	2,087	392	2,274	2,666	1,233	7,435	151,8	0,374 7	640	2,107
85	95,2	1,972	399	2,270	2,669	1,252	7,415	152,6	0,361 1	647	2,103
90	96,7	1,869	405	2,266	2,671	1,270	7,395	154,8	0,348 5	653	2,098
95	98,2	1,777	412	2,262	2,674	1,287	7,377	156,8	0,336 7	659	2,094
100	99,6	1,694	418	2,258	2,676	1,303	7,360	158,2	0,326 7	665	2,089
110	102,3	1,549	429	2,251	2,680	1,333	7,328	157,5	0,315 5	670	2,085
120	104,8	1,428	439	2,244	2,683	1,361	7,300	160,1	0,305 9	676	2,081
130	107,1	1,325	449	2,238	2,687	1,387	7,272	161,4	0,296 8	682	2,077
140	109,3	1,236	458	2,232	2,690	1,411	7,247	162,6	0,288 3	687	2,073
150	111,4	1,159	467	2,226	2,693	1,434	7,223	163,8	0,280 3	692	2,069
160	113,3	1,091	475	2,221	2,696	1,455	7,202	165,0	0,272 7	697	2,065
170	115,2	1,031	483	2,216	2,699	1,475	7,181	166,1	0,265 5	702	2,061
180	116,9	977,2	491	2,211	2,702	1,494	7,162	167,2	0,258 7	707	2,057
190	118,6	929,0	498	2,206	2,704	1,513	7,144	172,5	0,252 2	712	2,054
200	120,2	885,4	505	2,202	2,707	1,530	7,127	173,4	0,246 1	717	2,050
210	121,8	835,9	511	2,197	2,708	1,547	7,111	174,4	0,240 3	721	2,047
220	123,3	809,8	518	2,193	2,711	1,563	7,095	175,4	0,234 7	725	2,043
230	124,7	776,8	524	2,189	2,713	1,578	7,080	176,3	0,229 4	730	2,040
240	126,1	746,5	530	2,185	2,715	1,593	7,066	177,2	0,224 3	734	2,036
250	127,4	718,4	535	2,181	2,716	1,607	7,052	178,1	0,219 5	739	2,033
260	128,7	692,5	541	2,177	2,718	1,621	7,039	179,0	0,214 8	743	2,030
270	130,0	668,4	546	2,174	2,720	1,634	7,026	179,9	0,210 4	747	2,026
280	131,2	646,0	551	2,170	2,721	1,647	7,014	180,8	0,185 5	751	2,023
290	132,4	625,1	557	2,167	2,724	1,660	7,002	181,7	0,177 4	781	2,020
300	133,5	605,6	561	2,163	2,724	1,672	6,991	182,6	0,170 0	790	2,017
310	134,7	587,2	566	2,160	2,726	1,683	6,980	183,5	0,163 2	798	2,014
320	135,8	570,0	571	2,157	2,728	1,695	6,969	184,4	0,155 9	807	2,006
330	136,8	553,8	576	2,154	2,730	1,706	6,959	185,3	0,147 1	815	2,003
340	137,9	538,5	580	2,150	2,730	1,717	6,949	186,2	0,138 4	823	2,000
350	138,9	524,0	584	2,147	2,731	1,727	6,939	187,1	0,129 7	831	1,997
360	139,9	510,3	589	2,144	2,733	1,738	6,930	188,0	0,121 0	839	1,994
370	140,8	497,4	593	2,141	2,734	1,748	6,921	189,8	0,112 7	847	1,991

$\rho$	$t_s$	$v_g$	$h_g$	$s_i$	$s_v$	$p$	$t_s$	$v_g$	$h_g$	$s_i$	$s_v$
kPa	°C	m³/kg	kJ/kg	kJ/kg	kJ/kg	kPa	°C	m³/kg	kJ/kg	kJ/kg	kJ/kg
32	70,6	4,922	296	2,332	2,628	0,962	7,747	141,8	0,485 1	597	2,139
34	72,0	4,650	302	2,329	2,631	0,980	7,727	142,7	0,473 4	601	2,136
36	73,4	4,408	307	2,326	2,633	0,996	7,707	143,6	0,462 2	605	2,133
38	74,7	4,190	313	2,322	2,635	1,011	7,688	144,5	0,451 6	609	2,130
40	75,9	3,993	318	2,319	2,637	1,026	7,671	145,4	0,441 5	612	2,128
45	78,7	3,576	330	2,312	2,642	1,060	7,631	146,3	0,431 8	616	2,125
50	81,4	3,240	341	2,305	2,646	1,091	7,595	147,1	0,422 6	620	2,122
55	83,7	2,964	351	2,299	2,650	1,119	7,562	147,9	0,413 8	624	2,120
60	86,0	2,732	360	2,294	2,654	1,145	7,533	148,7	0,405 3	627	2,117
65	88,0	2,535	369	2,288	2,657	1,170	7,506	149,5	0,397 2	630	2,115
70	90,0	2,365	377	2,283	2,660	1,192	7,480	150,3	0,389 4	634	2,112
75	91,8	2,217	385	2,279	2,664	1,213	7,457	151,1	0,381 9	637	2,110
80	93,5	2,087	392	2,274	2,666	1,233	7,435	151,8	0,374 7	640	2,107
85	95,2	1,972	399	2,270	2,669	1,252	7,415	152,6	0,361 1	647	2,103
90	96,7	1,869	405	2,266	2,671	1,270	7,395	154,8	0,348 5	653	2,098
95	98,2	1,777	412	2,262	2,674	1,287	7,377	156,8	0,336 7	659	2,094
100	99,6	1,694	418	2,258	2,676	1,303	7,360	158,2	0,326 7	665	2,089
110	102,3	1,549	429	2,251	2,680	1,333	7,328	159,8	0,315 5	670	2,085
120	104,8	1,428	439	2,244	2,683	1,361	7,300	160,1	0,305 9	676	2,081
130	107,1	1,325	449	2,238	2,687	1,387	7,272	161,4	0,296 8	682	2,077
140	109,3	1,236	458	2,232	2,690	1,411	7,247	162,6	0,288 3	687	2,073
150	111,4	1,159	467	2,226	2,693	1,434	7,223	163,8	0,280 3	692	2,069
160	113,3	1,091	475	2,221	2,696	1,455	7,202	165,0	0,272 7	697	2,065
170	115,2	1,031	483	2,216	2,699	1,475	7,181	166,1	0,265 5	702	2,061
180	116,9	977,2	491	2,211	2,702	1,494	7,162	167,2	0,258 7	707	2,057
190	118,6	929,0	498	2,206	2,704	1,513	7,144	168,3	0,252 2	712	2,054
200	120,2	885,4	505	2,202	2,707	1,530	7,127	169,4	0,246 1	717	2,050
210	121,8	835,9	511	2,197	2,708	1,547	7,111	170,4	0,240 3	721	2,047
220	123,3	809,8	518	2,193	2,711	1,563	7,095	171,4	0,234 7	725	2,043
230	124,7	776,8	524	2,189	2,713	1,578	7,080	172,5	0,229 4	730	2,040
240	126,1	746,5	530	2,185	2,715	1,593	7,066	173,4	0,224 3	734	2,036
250	127,4	718,4	535	2,181	2,716	1,607	7,052	174,4	0,219 5	739	2,033
260	128,7	692,5	541	2,177	2,718	1,621	7,039	175,4	0,214 8	743	2,030
270	130,0	668,4	546	2,174	2,720	1,634	7,026	176,3	0,210 4	747	2,026
280	131,2	646,0	551	2,170	2,721	1,647	7,014	177,2	0,206 1	751	2,023
290	132,4	625,1	557	2,167	2,724	1,660	7,002	178,1	0,202 0	755	2,020
300	133,5	605,6	561	2,177	2,724	1,672	6,991	179,0	0,198 1	759	2,017
310	134,7	587,2	566	2,174	2,726	1,683	6,980	180,0	0,194 3	763	2,014
320	135,8	570,0	571	2,157	2,728						

$\rho$	$t_s$	$v_v$	$h_i$	$h_g$	$s_i$	$s_g$
kPa	°C	m³/kg	kJ/kg	kJ/kg	kJ/kg,K	kJ/kg,K
1 350	-193,4	0,145 7	823	1 964	2 787	2,268
1 400	-195,0	0,140 7	830	1 958	2 768	2,284
1 450	-196,7	0,136 0	838	1 951	2 769	2,299
1 500	-198,3	0,131 7	845	1 945	2 790	2,315
1 550	-199,9	0,127 5	852	1 939	2 791	2,330
1 600	-201,4	0,123 7	859	1 933	2 792	2,344
1 650	-202,9	0,120 1	865	1 927	2 792	2,358
1 700	-204,3	0,116 6	872	1 922	2 784	2,371
1 750	-205,7	0,113 4	878	1 916	2 794	2,385
1 800	-207,1	0,110 3	885	1 910	2 795	2,398
1 850	-208,5	0,107 4	891	1 905	2 796	2,410
1 900	-209,8	0,104 7	897	1 899	2 796	2,423
1 950	-211,1	0,102 0	903	1 894	2 797	2,435
2 000	-212,4	0,099 54	908	1 889	2 797	2,447
2 050	-213,6	0,097 16	914	1 883	2 797	2,459
2 100	-214,9	0,094 89	920	1 878	2 798	2,470
2 150	-216,1	0,092 72	926	1 873	2 799	2,481
2 200	-217,2	0,090 65	931	1 868	2 799	2,492
2 250	-218,4	0,088 67	936	1 863	2 799	2,503
2 300	-219,6	0,086 77	942	1 858	2 800	2,514
2 350	-220,7	0,084 95	947	1 853	2 800	2,524
2 400	-221,8	0,083 20	952	1 849	2 801	2,534
2 450	-222,9	0,081 52	957	1 844	2 801	2,544
2 500	-223,9	0,079 91	962	1 839	2 801	2,554
2 550	-225,0	0,078 35	967	1 834	2 801	2,564
2 600	-226,0	0,076 86	972	1 830	2 802	2,574
2 650	-227,1	0,075 41	977	1 825	2 802	2,583
2 700	-228,1	0,074 02	981	1 821	2 802	2,592
2 750	-229,1	0,072 68	986	1 816	2 802	2,602
2 800	-230,1	0,071 39	991	1 811	2 802	2,611
2 850	-231,0	0,070 14	995	1 807	2 802	2,620
2 900	-232,0	0,068 93	1 000	1 802	2 802	2,628
2 950	-232,9	0,067 76	1 004	1 798	2 802	2,637
3 000	-233,8	0,066 63	1 008	1 794	2 802	2,646
3 100	-235,7	0,064 47	1 017	1 785	2 802	2,662
3 200	-237,5	0,062 44	1 025	1 777	2 802	2,679
3 300	-239,2	0,060 53	1 034	1 768	2 802	2,695
3 400	-240,9	0,058 73	1 042	1 760	2 802	2,710
3 500	-242,5	0,057 03	1 050	1 752	2 802	2,725
3 600	-244,2	0,055 41	1 058	1 744	2 802	2,740
3 700	-245,8	0,053 89	1 065	1 736	2 801	2,755
3 800	-247,3	0,052 44	1 073	1 728	2 801	2,769
3 900	-248,8	0,051 06	1 080	1 721	2 801	2,783
4 000	-250,3	0,049 75	1 087	1 713	2 800	2,797

$\rho$	$t_s$	$v_v$	$h_i$	$h_g$	$s_i$	$s_g$
kPa	°C	m³/kg	kJ/kg	kJ/kg	kJ/kg,K	kJ/kg,K
4 100	-251,8	0,048 50	1 095	1 705	2 800	2,810
4 200	-253,2	0,047 31	1 102	1 698	2 800	2,823
4 300	-254,7	0,046 17	1 109	1 690	2 799	2,836
4 400	-256,1	0,045 08	1 115	1 683	2 798	2,849
4 500	-257,4	0,044 04	1 122	1 676	2 798	2,861
4 600	-258,8	0,043 04	1 129	1 668	2 797	2,874
4 700	-260,1	0,042 08	1 135	1 661	2 796	2,886
4 800	-261,4	0,041 16	1 142	1 654	2 796	2,897
4 900	-262,7	0,040 28	1 148	1 647	2 795	2,909
5 000	-263,9	0,039 43	1 155	1 640	2 795	2,921
5 100	-265,2	0,038 61	1 161	1 633	2 794	2,932
5 200	-266,4	0,037 82	1 167	1 626	2 793	2,943
5 300	-267,6	0,037 07	1 173	1 619	2 792	2,954
5 400	-268,8	0,036 33	1 179	1 612	2 791	2,965
5 500	-269,9	0,035 63	1 185	1 605	2 790	2,976
5 600	-271,1	0,034 95	1 191	1 598	2 789	2,986
5 700	-272,2	0,034 29	1 197	1 591	2 788	2,997
5 800	-273,4	0,033 65	1 202	1 585	2 787	3,007
5 900	-274,5	0,033 03	1 208	1 578	2 786	3,017
6 000	-275,6	0,032 44	1 214	1 571	2 785	3,027
6 200	-277,7	0,031 30	1 225	1 558	2 783	3,047
6 400	-279,8	0,030 23	1 236	1 545	2 781	3,066
6 600	-281,8	0,029 22	1 247	1 532	2 779	3,085
6 800	-283,8	0,028 27	1 257	1 519	2 776	3,104
7 000	-285,8	0,027 37	1 267	1 506	2 773	3,122
7 200	-287,7	0,026 52	1 278	1 493	2 771	3,140
7 400	-289,6	0,025 72	1 288	1 481	2 769	3,157
7 600	-291,4	0,024 95	1 298	1 468	2 766	3,174
7 800	-293,2	0,024 22	1 307	1 455	2 762	3,191
8 000	-295,0	0,023 53	1 317	1 443	2 760	3,208
8 200	-296,7	0,022 86	1 327	1 430	2 757	3,224
8 400	-298,4	0,022 23	1 336	1 418	2 754	3,240
8 600	-300,1	0,021 63	1 345	1 406	2 751	3,256
8 800	-301,7	0,021 05	1 355	1 393	2 748	3,271
9 000	-303,3	0,020 50	1 364	1 381	2 745	3,287
9 200	-304,9	0,019 96	1 373	1 369	2 742	3,302
9 400	-306,4	0,019 45	1 382	1 356	2 738	3,317
9 600	-308,0	0,018 97	1 391	1 344	2 735	3,332
9 800	-309,5	0,018 49	1 399	1 332	2 731	3,346
10 000	-311,0	0,018 04	1 408	1 320	2 728	3,361
10 400	-313,4	0,017 18	1 425	1 295	2 720	3,389
10 800	-316,7	0,016 39	1 442	1 271	2 713	3,417
11 200	-319,4	0,015 64	1 459	1 247	2 706	3,444
11 600	-322,1	0,014 94	1 475	1 222	2 697	3,471

## Properties of Superheated Steam

$P$ kPa	$t_s$ °C	$v_g$ m³/kg	$h_i$ kJ/kg	$h_{fo}$ kJ/kg	$h_o$ kJ/kg	$s_i$ kJ/kg,K	$s_o$ kJ/kg,K
12 000	324,7	0,014 28	1 492	1 197	2 689	3,497	5,500
12 400	327,2	0,013 66	1 508	1 173	2 681	3,523	5,477
12 800	329,6	0,013 08	1 524	1 148	2 672	3,549	5,453
13 200	332,0	0,012 52	1 540	1 122	2 662	3,574	5,429
13 600	334,4	0,012 00	1 556	1 097	2 653	3,599	5,405
14 000	336,6	0,011 50	1 572	1 071	2 643	3,624	5,380
14 400	338,9	0,011 02	1 587	1 044	2 631	3,649	5,356
14 800	341,1	0,010 56	1 603	1 018	2 621	3,674	5,331
15 200	343,2	0,010 12	1 619	990	2 609	3,698	5,305
15 600	345,3	0,009 707	1 635	963	2 598	3,723	5,279
16 000	347,3	0,009 308	1 651	934	2 585	3,747	5,253
16 400	349,3	0,008 925	1 667	906	2 573	3,772	5,227
16 800	351,3	0,008 553	1 683	876	2 559	3,797	5,199
17 200	353,2	0,008 191	1 700	844	2 544	3,824	5,171
17 600	355,1	0,007 839	1 718	812	2 530	3,850	5,143
18 000	357,0	0,007 498	1 735	779	2 514	3,877	5,113
18 400	358,8	0,007 165	1 752	745	2 497	3,903	5,082
18 800	360,6	0,006 839	1 770	710	2 480	3,929	5,050
19 200	362,3	0,006 517	1 788	673	2 461	3,957	5,016
19 600	364,0	0,006 198	1 807	634	2 441	3,985	4,980
20 000	365,7	0,005 877	1 827	592	2 419	4,015	4,941

$P$ kPa	$t_{sup}$	$t_{sup}$					
		$V_{sup}$	$h_{sup}$	$s_{sup}$	$V_{sup}$	$h_{sup}$	$s_{sup}$
1	149,1	172,2	195,3	218,4	241,4	264,5	310,7
	2 595	2 689	2 784	2 880	2 978	3 077	3 280
	9,512	9,751	9,986	10,163	10,344	10,670	10,960
5	29,78	34,42	39,04	43,68	48,28	52,90	62,13
	2 594	2 688	2 784	2 880	2 978	3 077	3 280
	8,496	8,768	9,008	9,223	9,420	9,601	9,927
10	14,87	17,20	19,51	21,88	24,14	26,45	31,06
	2 592	2 688	2 783	2 880	2 977	3 077	3 280
	8,173	8,447	8,688	8,903	9,100	9,281	9,607
50	3,420	3,890	4,356	4,821	5,284	6,209	7,134
	2 683	2 780	2 878	2 976	3 076	3 279	3 486
	7,694	7,940	8,158	8,355	8,537	8,864	9,154
75	2,271	2,588	2,901	3,211	3,521	4,138	4,755
	2 680	2 779	2 877	2,975	3 075	3 279	3 489
	7,500	7,750	7,968	8,167	8,349	8,676	8,967
100	1,696	1,937	2,173	2,406	2,639	3,103	3,565
	2 676	2 777	2 876	2,976	3 076	3 278	3 488
	7,36	7,614	7,834	8,033	8,215	8,543	8,834
150	1,266	1,445	1,601	1,757	2,007	2,376	
	2 773	2 873	2,973	3 073	3 277	3 488	
	7,420	7,643	7,843	8,027	8,355	8,646	
200	0,960 2	1,081	1,199	1,316	1,549	1,781	
	2 770	2 871	2,971	3 072	3 277	3 487	
	7,280	7,507	7,708	7,892	8,221	8,513	
300	0,634 2	0,716 6	0,796 5	0,875 4	1,031	1,187	
	2 762	2 866	2,968	3 070	3 275	3 486	
	7,078	7,312	7,517	7,702	8,032	8,324	
400	0,471	0,534 5	0,654 9	0,772 5	0,889 3	0,988 3	
	2 753	2 862	2,965	3 067	3 274	3 485	
	6,929	7,172	7,379	7,566	7,898	8,191	

$P$ kPa	$t_{sup}$							$t_{sup}$	
		200°	250°	300°	350°	400°	450°		
500	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,425 2 2 857 7,060	0,474 5 2 962 7,271	0,522 6 3 065 7,460	0,570 1 3 168 7,633	0,617 2 3 272 7,783	0,664 1 3 377 7,944	0,710 8 3 484 8,087	0,804 3 702 8,351
600	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,352 2 2 851 6,966	0,394 2 958 7,162	0,444 4 3 082 7,373	0,474 3 3 166 7,546	0,513 6 3 270 7,707	0,552 8 3 378 7,858	0,591 9 3 483 8,001	0,869 7 3 701 8,267
700	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,300 1 2 846 6,888	0,336 4 2 955 7,106	0,371 4 3 060 7,288	0,405 8 3 164 7,473	0,439 7 3 269 7,634	0,473 4 3 374 7,786	0,506 9 3 482 8,195	0,573 7 3 700 8,320
800	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,261 2 840 6,817	0,293 3 2 951 7,040	0,324 2 3 057 7,233	0,354 4 3 162 7,409	0,384 2 3 267 7,571	0,413 8 3 373 7,723	0,443 2 3 480 8,132	0,501 8 3 689 8,369
900	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,230 5 2 835 6,753	0,259 7 2 948 6,980	0,287 4 3 055 7,176	0,314 4 3 160 7,352	0,341 3 266 7,515	0,367 4 3 372 7,667	0,393 7 3 480 7,811	0,445 8 3 689 8,077
1 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,206 1 2 829 6,695	0,232 8 2 944 6,926	0,258 3 052 7,124	0,282 5 3 158 7,301	0,306 5 3 284 7,464	0,330 3 3 370 7,617	0,354 3 478 7,761	0,401 3 698 8,028
1 500	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,132 4 2 786 6,452	0,152 2 925 6,711	0,169 7 3 039 6,919	0,186 5 3 148 7,102	0,202 9 3 256 7,266	0,219 1 3 364 7,423	0,235 1 3 473 7,569	0,266 7 3 694 7,838
2 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,111 5 2 904 6,547	0,125 5 3 025 6,768	0,138 6 3 138 6,957	0,151 1 3 248 7,126	0,163 4 3 357 7,283	0,175 6 3 467 7,481	0,199 5 3 690 7,701	0,226 7 3 900 7,938
3 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,070 6 2 858 6,289	0,081 2 3 025 6,541	0,090 5 3 117 6,744	0,099 3 3 214 7,126	0,107 8 3 330 7,283	0,116 1 3 445 7,507	0,132 4 3 682 7,701	0,175 6 3 900 7,938
4 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,058 8 2 963 6,364	0,066 4 3 094 6,541	0,077 3 3 117 6,744	0,090 3 3 214 7,126	0,098 4 3 330 7,283	0,107 8 3 445 7,507	0,122 4 3 682 7,701	0,175 6 3 900 7,938
5 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,045 3 2 927 6,212	0,051 9 3 070 6,451	0,057 8 3 117 6,646	0,063 2 3 214 6,818	0,068 5 3 330 6,975	0,076 6 3 445 7,268	0,098 6 3 682 7,368	0,122 4 3 900 7,938
6 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,036 2 2 887 6,071	0,042 2 3 045 6,336	0,047 3 3 070 6,451	0,052 1 3 196 6,646	0,058 2 3 316 6,818	0,068 5 3 433 6,975	0,076 6 3 666 7,268	0,122 4 3 900 7,938
7 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,029 5 2 841 5,934	0,035 2 3 018 6,231	0,039 9 3 158 6,448	0,044 1 3 287 6,632	0,048 1 3 410 6,796	0,055 6 3 649 7,008	0,062 1 3 819 6,904	0,122 4 3 900 7,938

$P$ kPa	$t_{sup}$							$t_{sup}$
		350°	375°	400°	425°	450°	500°	
8 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,029 94 2 990 6,133	0,032 2 3 067 6,255	0,034 28 3 139 6,384	0,036 25 3 207 6,483	0,038 12 3 272 6,555	0,041 17 3 338 6,641	0,048 39 3 401 6,729
9 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,025 78 2 959 6,039	0,027 94 3 042 6,171	0,029 91 3 118 6,286	0,031 73 3 189 6,385	0,036 73 3 256 6,484	0,042 79 3 321 6,557	0,048 52 3 393 6,720
10 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,022 41 2 926 5,947	0,024 53 3 017 6,091	0,026 39 3 087 6,213	0,028 12 3 172 6,321	0,029 72 3 241 6,419	0,032 75 3 313 6,500	0,038 31 3 386 6,666
11 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,019 6 2 889 5,856	0,021 69 2 989 6,014	0,023 5 3 075 6,143	0,026 66 3 153 6,257	0,026 66 3 225 6,358	0,029 49 3 300 6,439	0,034 65 3 360 6,500
12 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,017 19 2 849 5,752	0,021 31 2 940 5,937	0,022 65 3 052 6,076	0,024 1 3 134 6,195	0,026 77 3 209 6,301	0,031 59 3 288 6,487	0,036 05 3 348 6,607
13 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,015 09 2 804 5,664	0,017 26 2 929 5,862	0,019 01 3 028 6,136	0,021 93 3 114 6,246	0,024 47 3 192 6,346	0,029 01 3 235 6,437	0,033 18 3 335 6,556
14 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,013 21 2 753 5,559	0,015 48 2 856 5,784	0,017 22 3 003 6,946	0,020 72 3 093 6,079	0,022 5 3 175 6,193	0,026 79 3 222 6,390	0,030 71 3 300 6,476
15 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,011 46 2 693 5,443	0,013 91 2 861 5,707	0,015 66 2 977 5,883	0,017 14 3 073 6,023	0,022 55 3 157 6,142	0,026 87 3 205 6,345	0,030 37 3 295 6,435
16 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,009 76 2 617 5,304	0,012 48 2 861 5,626	0,014 27 2 977 5,820	0,017 33 3 073 6,023	0,023 19 3 157 6,142	0,026 78 3 205 6,345	0,030 37 3 295 6,435
17 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,011 17 2 778 5,541	0,013 03 2 986 5,756	0,014 49 3 094 5,914	0,017 96 3 189 6,093	0,021 71 3 256 6,200	0,023 19 3 309 6,301	0,025 06 3 360 6,399
18 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,009 97 2 729 5,541	0,011 91 2 986 5,756	0,013 38 3 094 5,914	0,016 78 3 189 6,093	0,021 71 3 256 6,200	0,023 39 3 328 6,301	0,025 06 3 386 6,399
19 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,008 82 2 674 5,449	0,010 89 2 855 5,691	0,012 38 3 082 5,861	0,013 62 3 102 5,997	0,015 72 3 121 6,219	0,021 71 3 281 6,321	0,022 26 3 345 6,425
20 000	$v_{sup}$ $h_{sup}$ $s_{sup}$	0,007 60 2 605 5,228	0,009 95 2 819 5,556	0,011 47 2 989 5,753	0,012 7 3 062 6,142	0,014 77 3 129 6,204	0,018 15 3 239 6,304	0,021 1 3 307 6,396

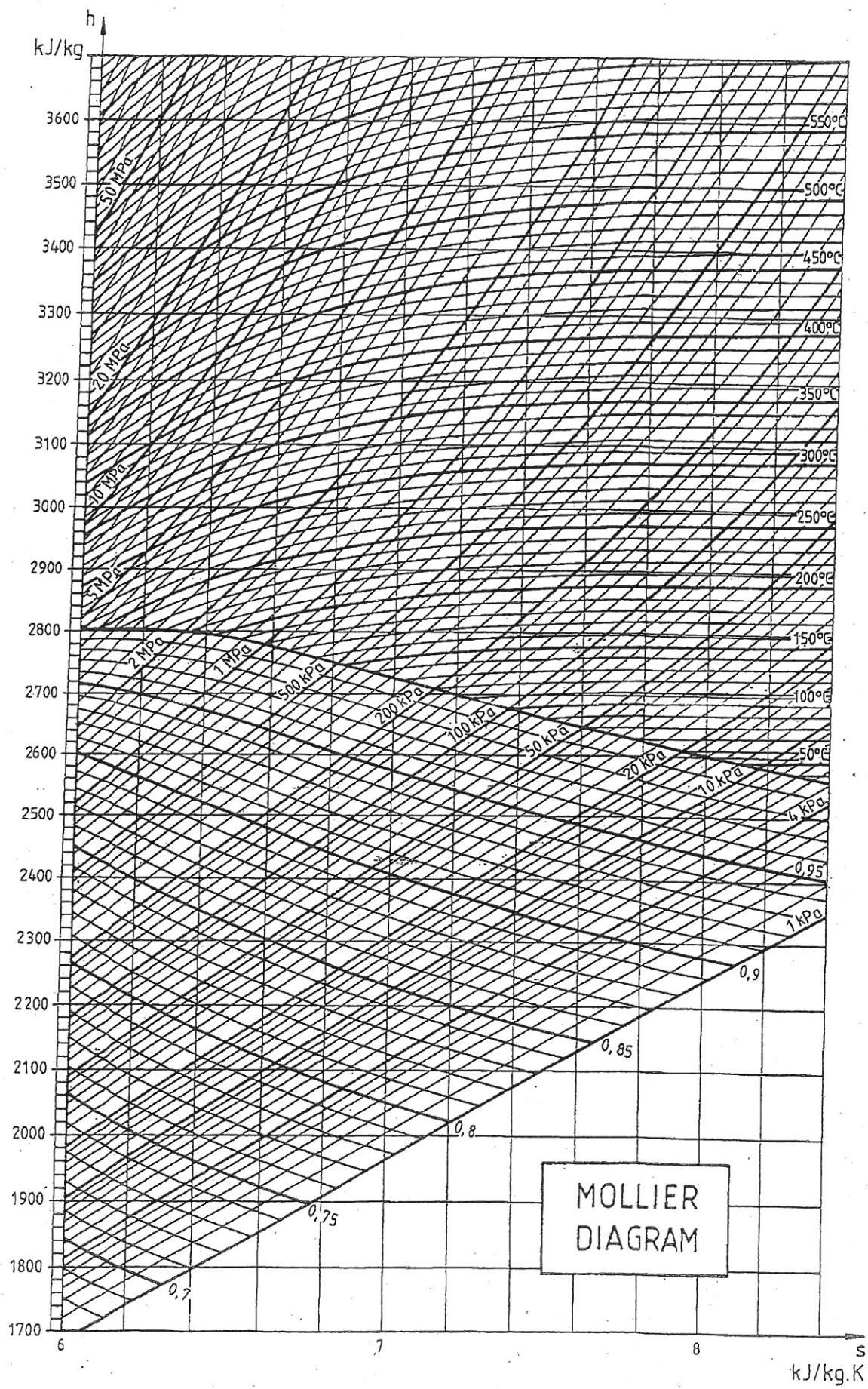


TABLE A-5

Saturated water—Pressure table

Press., <i>P</i> kPa	Specific volume, m <sup>3</sup> /kg			Internal energy, kJ/kg			Enthalpy, kJ/kg			Entropy, kJ/kg·K		
	Sat. temp., <i>T</i> <sub>sat</sub> °C	Sat. liquid, <i>v</i> <sub>f</sub>	Sat. vapor, <i>v</i> <sub>g</sub>	Sat. liquid, <i>u</i> <sub>f</sub>	Evap., <i>u</i> <sub>fg</sub>	Sat. vapor, <i>u</i> <sub>g</sub>	Sat. liquid, <i>h</i> <sub>f</sub>	Evap., <i>h</i> <sub>fg</sub>	Sat. vapor, <i>h</i> <sub>g</sub>	Sat. liquid, <i>s</i> <sub>f</sub>	Evap., <i>s</i> <sub>fg</sub>	Sat. vapor, <i>s</i> <sub>g</sub>
1.0	6.97	0.001000	129.19	29.302	2355.2	2384.5	29.303	2484.4	2513.7	0.1059	8.8690	8.9749
1.5	13.02	0.001001	87.964	54.686	2338.1	2392.8	54.688	2470.1	2524.7	0.1956	8.6314	8.8270
2.0	17.50	0.001001	66.990	73.431	2325.5	2398.9	73.433	2459.5	2532.9	0.2606	8.4621	8.7227
2.5	21.08	0.001002	54.242	88.422	2315.4	2403.8	88.424	2451.0	2539.4	0.3118	8.3302	8.6421
3.0	24.08	0.001003	45.654	100.98	2306.9	2407.9	100.98	2443.9	2544.8	0.3543	8.2222	8.5765
4.0	28.96	0.001004	34.791	121.39	2293.1	2414.5	121.39	2432.3	2553.7	0.4224	8.0510	8.4734
5.0	32.87	0.001005	28.185	137.75	2282.1	2419.8	137.75	2423.0	2560.7	0.4762	7.9176	8.3938
7.5	40.29	0.001008	19.233	168.74	2261.1	2429.8	168.75	2405.3	2574.0	0.5763	7.6738	8.2501
10	45.81	0.001010	14.670	191.79	2245.4	2437.2	191.81	2392.1	2583.9	0.6492	7.4996	8.1488
15	53.97	0.001014	10.020	225.93	2222.1	2448.0	225.94	2372.3	2598.3	0.7549	7.2522	8.0071
20	60.06	0.001017	7.6481	251.40	2204.6	2456.0	251.42	2357.5	2608.9	0.8320	7.0752	7.9073
25	64.96	0.001020	6.2034	271.93	2190.4	2462.4	271.96	2345.5	2617.5	0.8932	6.9370	7.8302
30	69.09	0.001022	5.2287	289.24	2178.5	2467.7	289.27	2335.3	2624.6	0.9441	6.8234	7.7675
40	75.86	0.001026	3.9933	317.58	2158.8	2476.3	317.62	2318.4	2636.1	1.0261	6.6430	7.6691
50	81.32	0.001030	3.2403	340.49	2142.7	2483.2	340.54	2304.7	2645.2	1.0912	6.5019	7.5931
75	91.76	0.001037	2.2172	384.36	2111.8	2496.1	384.44	2278.0	2662.4	1.2132	6.2426	7.4558
100	99.61	0.001043	1.6941	417.40	2088.2	2505.6	417.51	2257.5	2675.0	1.3028	6.0562	7.3589
101.325	99.97	0.001043	1.6734	418.95	2087.0	2506.0	419.06	2256.5	2675.6	1.3069	6.0476	7.3545
125	105.97	0.001048	1.3750	444.23	2068.8	2513.0	444.36	2240.6	2684.9	1.3741	5.9100	7.2841
150	111.35	0.001053	1.1594	466.97	2052.3	2519.2	467.13	2226.0	2693.1	1.4337	5.7894	7.2231
175	116.04	0.001057	1.0037	486.82	2037.7	2524.5	487.01	2213.1	2700.2	1.4850	5.6865	7.1716
200	120.21	0.001061	0.88578	504.50	2024.6	2529.1	504.71	2201.6	2706.3	1.5302	5.5968	7.1270
225	123.97	0.001064	0.79329	520.47	2012.7	2533.2	520.71	2191.0	2711.7	1.5706	5.5171	7.0877
250	127.41	0.001067	0.71873	535.08	2001.8	2536.8	535.35	2181.2	2716.5	1.6072	5.4453	7.0525
275	130.58	0.001070	0.65732	548.57	1991.6	2540.1	548.86	2172.0	2720.9	1.6408	5.3800	7.0207
300	133.52	0.001073	0.60582	561.11	1982.1	2543.2	561.43	2163.5	2724.9	1.6717	5.3200	6.9917
325	136.27	0.001076	0.56199	572.84	1973.1	2545.9	573.19	2155.4	2728.6	1.7005	5.2645	6.9650
350	138.86	0.001079	0.52422	583.89	1964.6	2548.5	584.26	2147.7	2732.0	1.7274	5.2128	6.9402
375	141.30	0.001081	0.49133	594.32	1956.6	2550.9	594.73	2140.4	2735.1	1.7526	5.1645	6.9171
400	143.61	0.001084	0.46242	604.22	1948.9	2553.1	604.66	2133.4	2738.1	1.7765	5.1191	6.8955
450	147.90	0.001088	0.41392	622.65	1934.5	2557.1	623.14	2120.3	2743.4	1.8205	5.0356	6.8561
500	151.83	0.001093	0.37483	639.54	1921.2	2560.7	640.09	2108.0	2748.1	1.8604	4.9603	6.8207
550	155.46	0.001097	0.34261	655.16	1908.8	2563.9	655.77	2096.6	2752.4	1.8970	4.8916	6.7886
600	158.83	0.001101	0.31560	669.72	1897.1	2566.8	670.38	2085.8	2756.2	1.9308	4.8285	6.7593
650	161.98	0.001104	0.29260	683.37	1886.1	2569.4	684.08	2075.5	2759.6	1.9623	4.7699	6.7322
700	164.95	0.001108	0.27278	696.23	1875.6	2571.8	697.00	2065.8	2762.8	1.9918	4.7153	6.7071
750	167.75	0.001111	0.25552	708.40	1865.6	2574.0	709.24	2056.4	2765.7	2.0195	4.6642	6.6837

### Saturated Water and Steam

t [°C]	$p_s$ [bar]	$v_g$ [m³/kg]	$h_f$	$h_{fg}$ [kJ/kg]	$h_g$	$s_f$	$s_{fg}$ [kJ/kg K]	$s_g$
0.01	0.006112	206.1	0*	2500.8	2500.8	0†	9.155	9.155
1	0.006566	192.6	4.2	2498.3	2502.5	0.015	9.113	9.128
2	0.007054	179.9	8.4	2495.9	2504.3	0.031	9.071	9.102
3	0.007575	168.2	12.6	2493.6	2506.2	0.046	9.030	9.076
4	0.008129	157.3	16.8	2491.3	2508.1	0.061	8.989	9.050
5	0.008719	147.1	21.0	2488.9	2509.9	0.076	8.948	9.024
6	0.009346	137.8	25.2	2486.6	2511.8	0.091	8.908	8.999
7	0.01001	129.1	29.4	2484.3	2513.7	0.106	8.868	8.974
8	0.01072	121.0	33.6	2481.9	2515.5	0.121	8.828	8.949
9	0.01147	113.4	37.8	2479.6	2517.4	0.136	8.788	8.924
10	0.01227	106.4	42.0	2477.2	2519.2	0.151	8.749	8.900
11	0.01312	99.90	46.2	2474.9	2521.1	0.166	8.710	8.876
12	0.01401	93.83	50.4	2472.5	2522.9	0.180	8.671	8.851
13	0.01497	88.17	54.6	2470.2	2524.8	0.195	8.633	8.828
14	0.01597	82.89	58.8	2467.8	2526.6	0.210	8.594	8.804
15	0.01704	77.97	62.9	2465.5	2528.4	0.224	8.556	8.780
16	0.01817	73.38	67.1	2463.1	2530.2	0.239	8.518	8.757
17	0.01936	69.09	71.3	2460.8	2532.1	0.253	8.481	8.734
18	0.02063	65.08	75.5	2458.4	2533.9	0.268	8.444	8.712
19	0.02196	61.34	79.7	2456.0	2535.7	0.282	8.407	8.689
20	0.02337	57.84	83.9	2453.7	2537.6	0.296	8.370	8.666
21	0.02486	54.56	88.0	2451.4	2539.4	0.310	8.334	8.644
22	0.02642	51.49	92.2	2449.0	2541.2	0.325	8.297	8.622
23	0.02808	48.62	96.4	2446.6	2543.0	0.339	8.261	8.600
24	0.02982	45.92	100.6	2444.2	2544.8	0.353	8.226	8.579
25	0.03166	43.40	104.8	2441.8	2546.6	0.367	8.190	8.557
26	0.03360	41.03	108.9	2439.5	2548.4	0.381	8.155	8.536
27	0.03564	38.81	113.1	2437.2	2550.3	0.395	8.120	8.515
28	0.03778	36.73	117.3	2434.8	2552.1	0.409	8.085	8.494
29	0.04004	34.77	121.5	2432.4	2553.9	0.423	8.050	8.473
30	0.04242	32.93	125.7	2430.0	2555.7	0.436	8.016	8.452
32	0.04754	29.57	134.0	2425.3	2559.3	0.464	7.948	8.412
34	0.05318	26.60	142.4	2420.5	2562.9	0.491	7.881	8.372
36	0.05940	23.97	150.7	2415.8	2566.5	0.518	7.814	8.332
38	0.06624	21.63	159.1	2411.0	2570.1	0.545	7.749	8.294
40	0.07375	19.55	167.5	2406.2	2573.7	0.572	7.684	8.256
42	0.08198	17.69	175.8	2401.4	2577.2	0.599	7.620	8.219
44	0.09100	16.03	184.2	2396.6	2580.8	0.625	7.557	8.182
46	0.1009	14.56	192.5	2391.8	2584.3	0.651	7.494	8.145
48	0.1116	13.23	200.9	2387.0	2587.9	0.678	7.433	8.111
50	0.1233	12.04	209.3	2382.1	2591.4	0.704	7.371	8.075
55	0.1574	9.578	230.2	2370.1	2600.3	0.768	7.223	7.991
60	0.1992	7.678	251.1	2357.9	2609.0	0.831	7.078	7.909
65	0.2501	6.201	272.0	2345.7	2617.7	0.893	6.937	7.830
70	0.3116	5.045	293.0	2333.3	2626.3	0.955	6.800	7.755
75	0.3855	4.133	313.9	2320.8	2634.7	1.015	6.666	7.681
80	0.4736	3.408	334.9	2308.3	2643.2	1.075	6.536	7.611
85	0.5780	2.828	355.9	2295.6	2651.5	1.134	6.410	7.544
90	0.7011	2.361	376.9	2282.8	2659.7	1.192	6.286	7.478
95	0.8453	1.982	398.0	2269.8	2667.8	1.250	6.166	7.416
100	1.01325	1.673	419.1	2256.7	2675.8	1.307	6.048	7.355

†  $u$  and  $s$  are chosen to be zero for saturated liquid at the triple point.

Note: values of  $v_f$  can be found on p. 10.

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