



PROGRAM : NATIONAL DIPLOMA
CHEMICAL ENGINEERING

SUBJECT : THERMODYNAMICS APPLIED 3111

CODE : ACT 3111

DATE : SUMMER EXAMINATION 2015
20 NOVEMBER 2015

DURATION : (SESSION 1) 08:30 - 11:30

WEIGHT : 40: 60

TOTAL MARKS : 100

EXAMINER : MRS TP MASHIFANA

MODERATOR : DR H RUTTO

NUMBER OF PAGES : 9 PAGES INCLUDING ANNEXURES

INSTRUCTIONS : QUESTION PAPERS MUST BE HANDED IN
: CALCULATORS ARE ALLOWED
: NO COMPUTERS ALLOWED
: NUMBER AND ANSWER ALL QUESTIONS IN AN ORDER
: UNIVERSITY EXAM RULES APPLY

Question 1**[40]**

1. The Carnot cycle is the most efficient ideal theoretical cycle. There are four steps that make up a *Carnot cycle*,

- 1.1. Name the four processes (4)
- 1.2. Show a T-s diagram for the cycle (3)
- 1.3. Show a P-v diagram for the cycle (3)

2. An oil engine takes in air at 1.5 bar, 30 °C and the maximum cycle pressure is 85 bar. The compression ratio is 16/1.

- 2.1. Draw a P-v diagram for the process (5)
- 2.2. Calculate the air standard thermal efficiency based on the dual-combustion cycle. (25)

Assume that heat added at constant volume is equal to heat added at constant pressure

Question 2**[15]**

A gas turbine has an overall pressure of 5 bar and a maximum cycle efficiency at 550 °C. The turbine drives the compressor and an electric generator, the mechanical efficiency of the drive is 97 %. The ambient temperature is 20 °C and air enters the compressor at a rate of 15 kg/s; the isentropic efficiencies of the compressor and turbine are 80 and 85 % respectively. Neglecting changes in kinetic energy, the mass flow rate of fuel and all pressure losses, calculate:

- 2.1. The power output (5)
- 2.2. The cycle efficiency (5)
- 2.3. The work ratio (5)

Question 3**[30]**

A compressor in the power turbine is driven by the HP turbine and the LP turbine drives a separate power shaft. Inlet temperature and pressure are 17 °C and 1.01 bar respectively and the pressure ratio is 8/1. The isentropic efficiencies of the compressor, the HP and LP turbines are 0.8, 0.85 and 0.83 respectively. The maximum temperature is 650 °C. $C_p = 1.005 \text{ kJ/kgK}$ and $\gamma = 1.4$ for the compression process, and $C_p = 1.15 \text{ kJ/kgK}$ and $\gamma = 1.33$ for the expansion process. Calculate:

- 3.1. The pressure and temperature of the gas entering the power turbine
- 3.2. Net power developed by the power turbine per kg/s of mass
- 3.3. The work ratio.
- 3.4. The thermal efficiency of a gas turbine unit.

A converge diverged nozzle expands air at 6.89 bar and 427 °C into a space at 1 bar. The throat area of the nozzle is 650 mm² and the exit area is 975 mm². The exit velocity is found to be 680 m/s where the inlet velocity is negligible. Assuming that friction in the converged portion is negligible, calculate:

- 4.1. The mass flow through the nozzle, stating whether the nozzle is under expanding or over expanding;
 - 4.2. The nozzle efficiency
 - 4.3. The coefficient of velocity
-

TOTAL MARKS = 100
FULL MARKS = 100

Formula Sheet

1. Carnot cycle:

$$\eta = \frac{W_{net}}{Q_1} = 1 - \frac{Q_2}{Q_1} = 1 - \frac{T_2}{T_1}$$

2. Constant pressure cycle:

$$\dot{m} = \frac{\dot{W}_{net}}{W_{net}}$$

Work ratio W:

$$W = 1 - \frac{T_1}{T_3} \left(\frac{P_2}{P_1} \right)^{(\gamma-1)/\gamma}$$

Gross work output = work output of HP turbine + work output of LP turbine

Adiabatic change in temperature

$$T_{i+1} = T_i \left(\frac{P_{i+1}}{P_i} \right)^{(\gamma-1)/\gamma}$$

3. Otto cycle thermal efficiency:

$$\eta = 1 - \frac{1}{\left(\frac{V_1}{V_2} \right)^{\gamma-1}}$$

4. Diesel cycle thermal efficiency:

$$\eta = 1 - \left(\frac{1}{V_1/V_2} \right)^{\gamma-1} \left\{ \frac{(V_3/V_2)^{\gamma-1}}{\gamma[(V_3/V_2)-1]} \right\}$$

5. Dual-combustion cycle:

$$\eta = 1 - \frac{C_v(T_5-T_1)}{C_v(T_3-T_2)+C_p(T_4-T_3)}$$

6. Mean effective pressure:

$$-W_{net} = P_m(V_1 - V_2)$$

7. Stirling and Ericsson cycles:

$$\eta_{Stirling} = \eta_{Ericsson} = \eta_{Carnot} = 1 - \frac{T_2}{T_1}$$

8. Rankine cycle pump work input:

$$W = v_i(P_{i+1} - P_i)$$

Expansion process

$$\text{Isentropic efficiency} = \frac{\text{actual work}}{\text{isentropic work}}$$

Compression process

$$\text{Isentropic efficiency} = \frac{\text{isentropic work}}{\text{actual work}}$$

9. For steam turbines:

$$\Delta C_w = C_{wi} + C_{we} = C_{re} \cos \beta_e + C_{ri} \cos \beta_i$$

Velocity coefficient :

$$k = \frac{C_{re}}{C_{ri}}$$

Diagram efficiency:

$$\eta_d = \frac{2C_b \Delta C_w}{C_{ai}^2}$$

Stage efficiency:

$$\eta_s = \frac{C_b \Delta C_w}{H_o - H_i}$$

Nozzle efficiency:

$$\eta_n = \frac{C_{ai}^2}{2(H_o - H_i)}$$

Driving force:

$$F_D = \dot{m} \Delta C_w$$

Power output:

$$\dot{W}_{output} = \dot{m} C_b \Delta C_w$$

End (Axial) thrust:

$$\text{Axial thrust} = \dot{m} \Delta C_f$$

where $\Delta C_f = C_{fi} - C_{fe} = C_{ri} \sin \beta_i - C_{re} \sin \beta_e$

and $\Delta C_w = C_{wi} + C_{we} = C_{re} \cos \beta_e + C_{ri} \cos \beta_i$

10. For Nozzles: Energy balance:

$$H_1 + \frac{C_1^2}{2} = H_2 + \frac{C_2^2}{2}$$

Critical pressure:

$$\frac{P_c}{P_1} = \left(\frac{2}{\gamma+1} \right)^{\gamma/(\gamma-1)}$$

Critical temperature:

$$\frac{T_c}{T_1} = \left(\frac{P_c}{P_1} \right)^{(\gamma-1)/\gamma}$$

Critical specific volume:

$$v_c = \frac{(R/M)T_c}{P_c}$$

Critical velocity:

$$C_c = \sqrt{\frac{\gamma R T_c}{M}} = \sqrt{2(H_1 - H_c)} = \sqrt{2C_p(T_1 - T_c)}$$

Exit specific volume: $v_2 = \frac{(R/M)T_2}{P_2}$

Exit velocity: $C_2 = \sqrt{2(H_1 - H_2)}$

Mass flowrate per unit area: $\frac{\dot{m}}{A_2} = \frac{C_2}{v_2}$

Nozzle efficiency: $Nozzle\ efficiency = \frac{H_1 - H_2}{H_1 - H_{2s}} = \frac{C_p(T_1 - T_2)}{C_p(T_1 - T_{2s})} = \frac{T_1 - T_2}{T_1 - T_{2s}}$

Velocity coefficient: $Velocity\ coefficient = \frac{C_2}{C_{2s}}$

Coefficient of discharge: $Coefficient\ of\ discharge = \frac{\dot{m}}{\dot{m}_s}$

For dry saturated steam $\gamma = 1.135$ & for superheated steam $\gamma = 1.3$

11. Refrigeration: Engine efficiency: $\eta_{carnot} = \frac{W_{net\ carnot\ engine}}{Q_1} = 1 - \frac{T_2}{T_1}$

Coefficient of Performance: $COP_{carnot} = \frac{Q_1\ refrigerator}{W_{refrigerator\ input}} = \frac{T_2}{T_1 - T_2}$

Table F.1 Saturated Steam, SI Units

<i>T</i> K	<i>P</i> kPa	SPECIFIC VOLUME <i>V</i>		INTERNAL ENERGY <i>U</i>		ENTHALPY <i>H</i>		ENTROPY <i>S</i>		
		sat. liq.	evap.	sat. liq.	evap.	sat. liq.	evap.	sat. liq.	evap.	
<i>V</i> = SPECIFIC VOLUME $\text{cm}^3 \text{g}^{-1}$										
<i>U</i> = SPECIFIC INTERNAL ENERGY kJ kg^{-1}										
<i>H</i> = SPECIFIC ENTHALPY kJ kg^{-1}										
<i>S</i> = SPECIFIC ENTROPY $\text{kJ kg}^{-1} \text{K}^{-1}$										
0	273.15	0.611	1.000	206300.	206300.	-0.04	2375.7	2375.6	-0.04	
1	273.16	0.611	1.000	206200.	206200.	0.00	2375.6	2375.6	0.00	
2	275.15	0.657	1.000	192600.	192600.	4.17	2376.9	2376.9	4.17	
3	276.15	0.757	1.000	179900.	179900.	8.39	2369.9	2378.3	8.39	
4	277.15	0.813	1.000	157300.	157300.	12.60	2367.1	2379.7	12.60	
5	278.15	0.872	1.000	147200.	147200.	16.80	2364.3	2381.1	16.80	
6	279.15	0.935	1.000	137800.	137800.	21.01	2361.4	2382.4	21.01	
7	280.15	1.001	1.000	129100.	129100.	25.21	2358.6	2383.8	25.21	
8	281.15	1.072	1.000	121000.	121000.	29.41	2355.8	2385.2	29.41	
9	282.15	1.147	1.000	113400.	113400.	33.60	2353.0	2386.6	33.60	
10	283.15	1.227	1.000	106400.	106400.	37.80	2350.1	2387.9	37.80	
11	284.15	1.312	1.000	99910.	99910.	41.99	2347.3	2389.3	41.99	
12	285.15	1.401	1.000	93830.	93830.	46.18	2344.5	2390.7	46.18	
13	286.15	1.497	1.001	88180.	88180.	50.38	2341.7	2392.1	50.38	
14	287.15	1.597	1.001	82900.	82900.	54.56	2338.9	2393.4	54.57	
15	288.15	1.704	1.002	77980.	77980.	58.75	2336.1	2394.6	58.75	
16	289.15	1.817	1.001	73380.	73380.	62.94	2333.2	2396.2	62.94	
17	290.15	1.936	1.001	69090.	69090.	67.12	2330.4	2397.6	67.13	
18	291.15	2.062	1.001	65090.	65090.	71.31	2327.6	2398.9	71.31	
19	292.15	2.196	1.002	61340.	61340.	75.49	2324.8	2400.3	75.50	
20	293.15	2.337	1.002	57840.	57840.	79.68	2322.0	2401.7	79.68	
21	294.15	2.485	1.002	54560.	54560.	83.86	2319.2	2403.0	83.86	
22	295.15	2.642	1.002	51490.	51490.	88.04	2316.4	2404.4	88.04	
23	296.15	2.808	1.002	48620.	48620.	92.22	2313.6	2405.8	92.23	
24	297.15	2.982	1.003	45930.	45930.	96.40	2310.7	2407.1	96.41	
25	298.15	3.166	1.003	43400.	43400.	100.6	2307.9	2408.5	100.6	
26	299.15	3.360	1.003	41030.	41030.	108.9	2302.3	2411.2	108.9	
27	300.15	3.564	1.003	38810.	38810.	113.1	2299.5	2412.6	113.1	
28	301.15	3.778	1.004	36730.	36730.	117.3	2296.7	2414.0	117.3	
29	302.15	4.004	1.004	34770.	34770.	121.5	2293.8	2415.3	121.5	

30	4.241	1.004	32930.	125.7	2291.0	2416.7	2430.7	2556.4	0.4365	8.0180	8.4546		
31	304.15	4.491	31200.	129.8	2288.2	2418.0	2428.3	2558.2	0.4503	7.9839	8.4342		
32	305.15	4.753	29570.	134.0	2285.4	2419.4	2425.9	2550.0	0.4640	7.9500	8.4140		
33	306.15	5.029	28040.	138.2	2282.6	2420.8	2423.6	2561.8	0.4777	7.9163	8.3939		
34	307.15	5.318	26600.	142.4	2279.7	2422.1	2421.2	2563.6	0.4913	7.8828	8.3740		
35	308.15	5.622	25240.	146.6	2276.9	2423.5	2416.6	2565.4	0.5049	7.8495	8.3543		
36	309.15	5.940	1.006	23970.	150.7	2274.1	2424.8	2416.4	2567.2	0.5184	7.8164	8.3348	
37	310.15	6.274	1.007	22760.	154.9	2271.3	2426.2	2414.1	2569.0	0.5319	7.7835	8.3154	
38	311.15	6.624	1.007	21630.	159.1	2268.4	2427.5	159.1	2411.7	2570.8	0.5453	7.7509	8.2962
39	312.15	6.991	1.007	20560.	163.3	2265.6	2428.9	163.3	2409.3	2572.6	0.5588	7.7184	8.2772
40	313.15	7.375	1.008	19550.	167.4	2262.8	2430.2	167.5	2406.9	2574.4	0.5721	7.6861	8.2583
41	314.15	7.777	1.008	18590.	171.6	2259.9	2431.6	171.6	2404.5	2576.2	0.5854	7.6541	8.2395
42	315.15	8.198	1.009	17690.	175.8	2257.1	2432.9	175.8	2402.1	2577.9	0.5987	7.6222	8.2209
43	316.15	8.639	1.009	16840.	180.0	2254.3	2434.2	180.0	2399.7	2579.7	0.6120	7.5905	8.2025
44	317.15	9.100	1.009	16040.	184.2	2251.4	2435.6	184.2	2397.3	2581.5	0.6252	7.5590	8.1842
45	318.15	9.582	1.010	15280.	188.3	2248.6	2436.9	188.4	2394.9	2583.3	0.6383	7.5277	8.1661
46	319.15	10.09	1.010	14580.	192.5	2245.7	2438.3	192.5	2392.5	2585.1	0.6514	7.4966	8.1481
47	320.15	10.61	1.011	13880.	196.7	2242.9	2439.6	196.7	2390.1	2586.9	0.6645	7.4657	8.1302
48	321.15	11.16	1.011	13230.	200.9	2240.0	2440.9	200.9	2387.7	2588.6	0.6776	7.4350	8.1125
49	322.15	11.74	1.012	12620.	205.1	2237.2	2442.3	205.1	2385.3	2590.4	0.6906	7.4044	8.0950
50	323.15	12.34	1.012	12040.	209.2	2234.3	2443.6	209.3	2382.9	2592.2	0.7035	7.3741	8.0776
51	324.15	12.96	1.013	11500.	213.4	2231.5	2444.9	213.4	2380.5	2593.9	0.7164	7.3439	8.0603
52	325.15	13.61	1.013	10980.	217.6	2228.6	2446.2	217.6	2378.1	2595.7	0.7283	7.3138	8.0432
53	326.15	14.29	1.014	10490.	221.8	2225.8	2447.6	221.8	2375.7	2597.5	0.7422	7.2840	8.0262
54	327.15	15.00	1.014	10020.	226.0	2222.9	2448.9	226.0	2373.2	2599.2	0.7550	7.2543	8.0093
55	328.15	15.74	1.015	9577.9	230.2	2220.0	2450.2	230.2	2370.8	2601.0	0.7677	7.2248	7.9925
56	329.15	16.51	1.015	9157.7	234.3	2217.2	2451.5	234.4	2368.4	2602.7	0.7804	7.1955	7.9759
57	330.15	17.31	1.016	8758.7	238.5	2214.3	2452.8	238.5	2365.9	2604.5	0.7931	7.1663	7.9595
58	331.15	18.15	1.016	8379.8	242.7	2211.4	2454.1	242.7	2363.5	2606.2	0.8058	7.1373	7.9431
59	332.15	19.02	1.017	8019.7	246.9	2208.6	2455.4	246.9	2361.1	2608.0	0.8184	7.1085	7.9269
60	333.15	19.92	1.017	7677.5	251.1	2205.7	2456.8	251.1	2358.6	2609.7	0.8310	7.0798	7.9108
61	334.15	20.86	1.018	7352.1	255.3	2202.8	2458.1	255.3	2356.2	2611.4	0.8435	7.0513	7.8948
62	335.15	21.84	1.018	7042.7	259.4	2199.9	2459.4	259.4	2353.7	2613.2	0.8560	7.0230	7.8790
63	336.15	22.86	1.019	6748.2	263.6	2197.0	2460.7	263.6	2351.3	2614.9	0.8685	6.9948	7.8833
64	337.15	23.91	1.019	6469.0	267.8	2194.1	2462.0	267.8	2348.8	2616.6	0.8805	6.9667	7.8477
65	338.15	25.01	1.020	6201.3	272.0	2191.2	2463.2	272.0	2346.3	2618.4	0.8933	6.9388	7.8222
66	339.15	26.15	1.020	5947.2	276.2	2188.3	2464.5	276.2	2343.9	2620.1	0.9057	6.9111	7.8168
67	340.15	27.33	1.021	5705.2	280.4	2185.4	2465.8	280.4	2341.4	2621.8	0.9180	6.8835	7.8015
68	341.15	28.56	1.022	5474.6	284.6	2182.5	2467.1	284.6	2338.9	2623.5	0.9303	6.8561	7.7864
69	342.15	29.84	1.022	5254.8	288.8	2179.6	2468.4	288.8	2336.4	2625.2	0.9426	6.8288	7.7714
70	343.15	31.16	1.023	5046.3	292.9	2176.7	2469.7	292.9	2334.0	2626.9	0.9548	6.8017	7.7565
71	344.15	32.53	1.023	4846.4	297.1	2173.8	2470.9	297.2	2331.5	2628.6	0.9670	6.7747	7.7417
72	345.15	33.96	1.024	4654.7	301.3	2170.9	2472.2	301.4	2329.0	2630.3	0.9792	6.7478	7.7270
73	346.15	35.43	1.025	4472.7	305.5	2168.0	2473.5	305.5	2326.5	2632.0	0.9913	6.7211	7.7124
74	347.15	36.96	1.025	4239.0	309.7	2165.1	2474.8	309.7	2324.0	2633.7	1.0034	6.6945	7.6979

Table F.2 Superheated Steam, SI Units

		TEMPERATURE: T kelvins (TEMPERATURE: $t^{\circ}\text{C}$)									
P/kPa	$T_{\text{sat}}/\text{K}(\text{at } f^{\circ}\text{C})$	sat. liq.	sat. vap.	348.15 (75)	373.15 (100)	398.15 (125)	423.15 (150)	448.15 (175)	473.15 (200)	498.15 (225)	523.15 (250)
1	280.13(6.98)	V	1.000	129200, 29.334	160640, 2385.2	172180, 2514.4	183720, 2552.3	195270, 2588.5	206810, 2624.9	218350, 2661.7	229890, 2698.8
10	318.98(45.83)	V	1.010	14670, 191.822	16030, 2438.0	17190, 2479.7	18350, 2515.6	19510, 2551.6	20660, 2624.5	21820, 2661.4	22980, 2698.6
20	333.24(60.09)	V	1.017	1649.8	8.1511	8.3168	8.4486	8.5722	8.7004	8.7994	8.9045
30	342.27(69.12)	V	1.022	5229.3	5322.0	5714.4	6104.6	6493.2	6880.8	7267.5	7653.8
40	349.04(75.89)	V	1.027	3993.4	4279.2	4573.3	4865.8	5157.2	5447.8	5738.0
50	354.50(81.35)	V	1.030	3240.2	4216.9	4712.6	5254.4	5866.2	6232.2	6660.3
75	364.94(91.79)	V	1.037	2496.7	2484.0	2682.6	2731.4	2780.9	2829.5	2878.2	2927.2
100	372.78(99.63)	V	1.043	1693.7	1693.7	1695.5	1816.7	1936.3	2054.7	2172.3	2289.4
		S	1.060	2506.1	2506.1	2506.6	2544.8	2582.7	2620.4	2658.1	2695.9
		S	1.0912	2675.4	2675.4	2676.2	2726.5	2776.3	2825.9	2875.4	2924.9
		S	1.3027	7.3598	7.3598	7.3618	7.4923	7.6137	7.7275	7.8349	7.9369

101.325	V	1.044	1673.0	1673.0	1792.7	1910.7	2027.7	2143.8	2259.3	2374.5
373.15(100.00)	H	418.959	2506.5	2506.5	2544.7	2582.6	2620.4	2658.1	2695.9	2735.9
	S	1.3069	2676.0	2676.0	2726.4	2776.2	2825.8	2875.3	2924.8	2974.5
		7.3554	7.3554	7.4860	7.6076	7.7213	7.8288	7.9308	8.0280	
125	V	1.049	1374.6	1374.6	1449.1	1545.6	1641.0	1735.6	1829.6	1923.2
379.14(105.99)	H	444.224	2513.4	2513.4	2542.9	2581.2	2619.3	2657.2	2695.2	2733.3
	S	444.356	2685.2	2685.2	2724.0	2774.4	2824.4	2874.2	2923.9	2973.7
384.52(111.37)	V	1.053	1159.0	1159.0	1204.0	1285.2	1365.2	1444.4	1523.0	1601.3
	H	466.968	2519.5	2519.5	2540.9	2579.7	2618.1	2656.3	2694.4	2732.7
	S	467.126	2683.4	2683.4	2721.5	2772.5	2822.9	2872.9	2922.9	2972.9
150	V	1.055	7.2847	7.2234	7.2953	7.4194	7.5352	7.6339	7.7324	7.8324
389.21(116.06)	H	486.815	2524.7	2524.7	1028.8	1099.1	1168.2	1236.4	1304.1	1371.3
	S	487.000	2700.3	2700.3	2538.9	2578.2	2616.9	2655.3	2693.7	2732.1
200	V	1.061	885.44	885.44	2719.0	2770.5	2821.3	2871.7	2921.9	2972.0
393.38(120.23)	H	504.489	2529.2	2529.2	2716.4	2768.5	2819.8	2870.5	2920.9	2971.2
	S	504.701	2706.3	2706.3	7.1523	7.2191	7.3447	7.4614	7.5708	7.6741
225	V	1.064	792.97	792.97	897.47	959.54	1020.4	1080.4	1139.8	1198.9
397.14(123.99)	H	520.465	2533.2	2533.2	2536.9	2576.6	2615.7	2654.4	2692.9	2731.4
	S	520.705	2711.6	2711.6	2713.8	2766.5	2818.2	2869.3	2919.9	2970.4
250	V	1.068	718.44	718.44	7.0928	7.2213	7.3400	7.4508	7.5551	7.6540
400.58(127.43)	H	535.343	2536.8	2536.8	7.1689	7.2794	7.3971	7.5072	7.6110	7.7096
	S	1.6071	2716.4	2716.4	7.1523	7.2191	7.3447	7.4614	7.5708	7.6741
275	V	1.071	657.04	657.04	795.25	850.97	905.44	959.06	1012.1	1064.7
403.75(130.60)	H	548.564	2540.0	2540.0	2534.8	2575.1	2614.5	2653.5	2692.2	2730.8
	S	548.858	2720.7	2720.7	2713.8	2766.5	2818.2	2868.0	2918.9	2969.6
300	V	1.073	605.56	605.56	7.0928	7.2213	7.3400	7.4508	7.5551	7.6540
406.69(133.54)	H	561.429	2543.0	2543.0	7.1689	7.2794	7.3971	7.5072	7.6110	7.7096
	S	1.6716	2724.7	2724.7	7.1523	7.2191	7.3447	7.4614	7.5708	7.6741
			6.9909	6.9909	7.0771	7.1990	7.3119	7.4177	7.5176	